

BRIDGE HEALTH MONITORING

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www.shm.ce.boun.edu.tr



Outline

- Structural Health Monitoring
- Some Recents Projects
- Bridge Health Monitoring

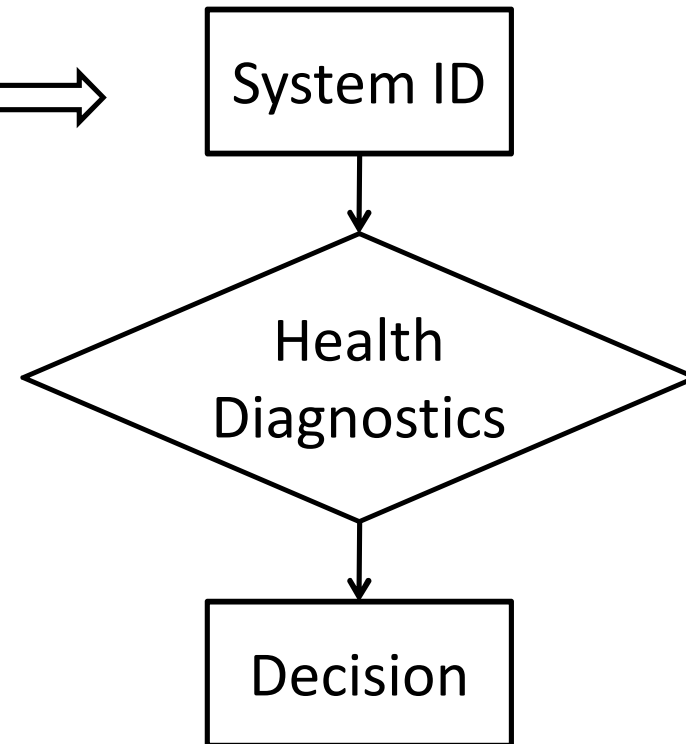
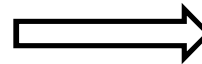
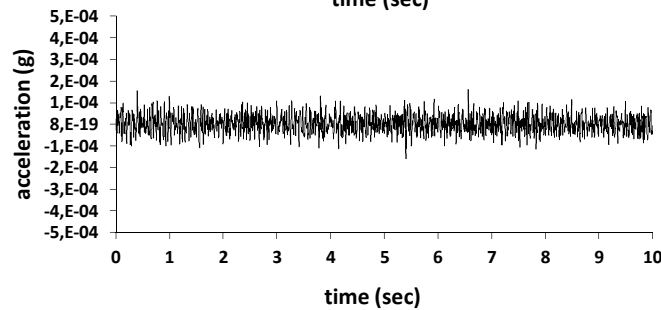
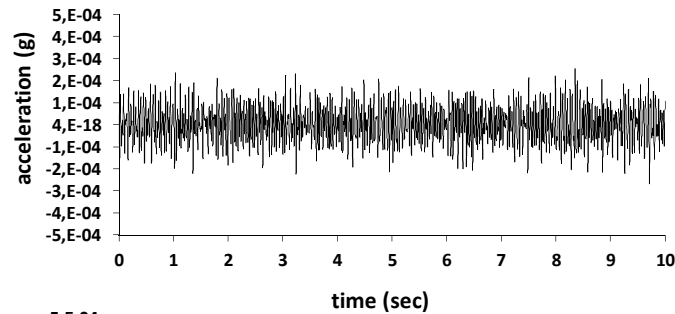
Vulnerability of Civil Infrastructure



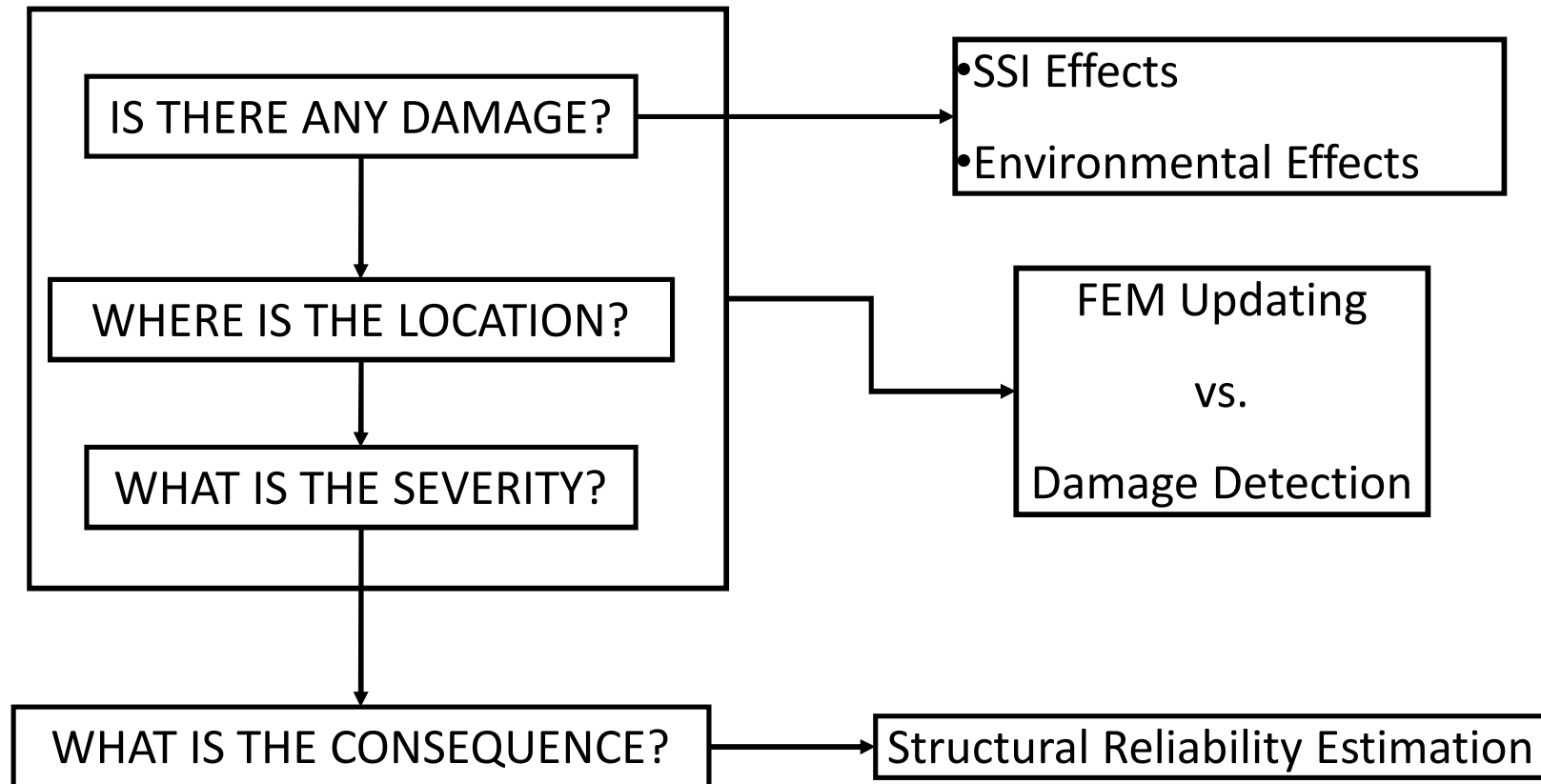
Visual Inspection



Vibration-Based Health Monitoring



SHM Flowchart



Outline

- Structural Health Monitoring

- Some Recents Projects

- SID of Historical Structures
- SID of RC Buildings
- SID of CFS Structures
- SID of a Chimney
- SHM of Offshore Platform
- SHM of a Wind Turbine
- SHM of a Tall Building

- Bridge Health Monitoring

Outline

- Structural Health Monitoring
- Some Recents Projects
- Bridge Health Monitoring
 - Highway Bridges
 - Historical Stone Arch Bridges
 - Suspension Bridges

Long-Term Monitoring of Jamboree Bridge

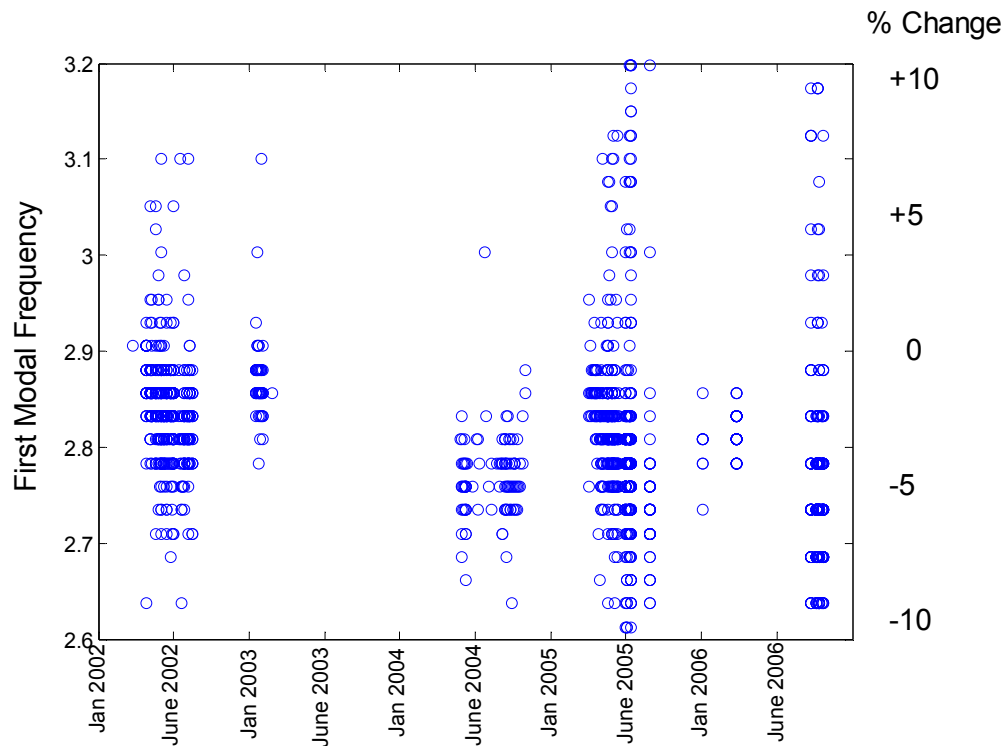


Soyoz S., Feng M.Q. (2009) “Long-term Monitoring and Identification of Bridge Structural Parameters” *Computer-Aided Civil and Infrastructure Engineering*, 24(2): 82-92.

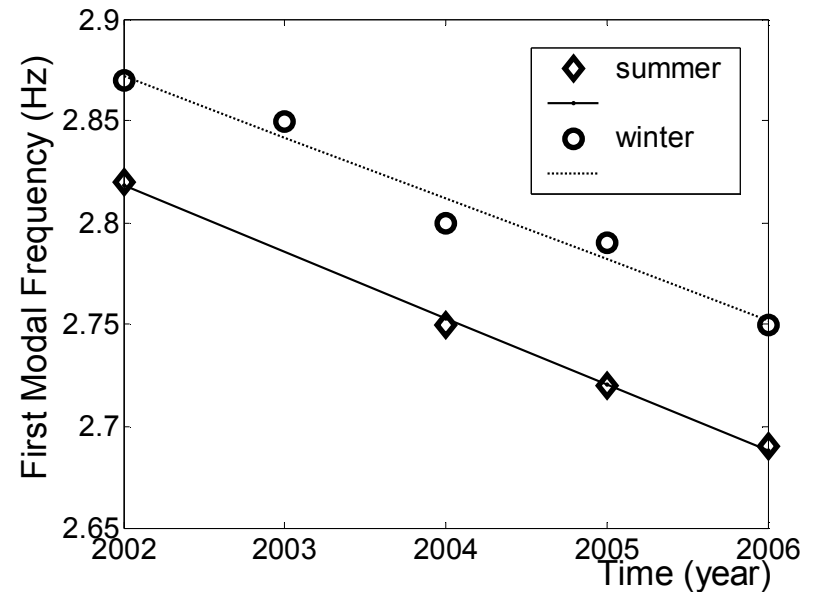
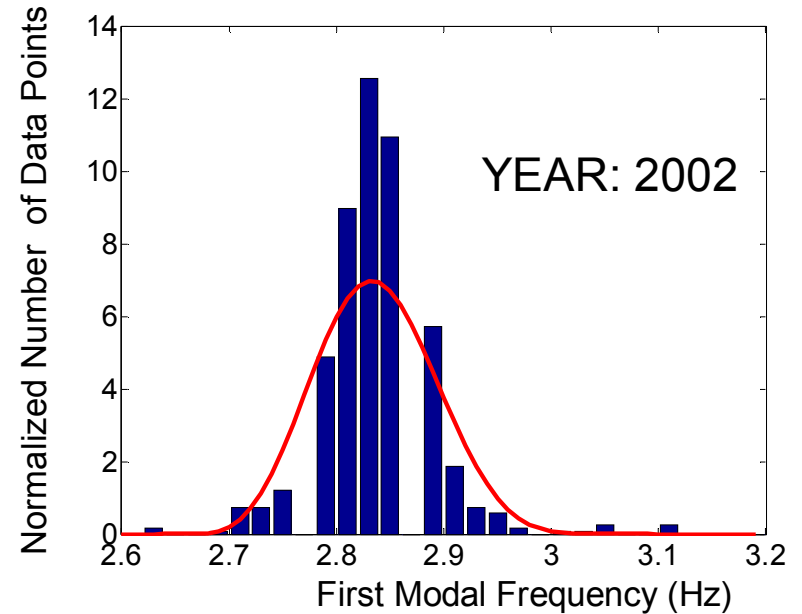
Remote Control and Data Acquisition



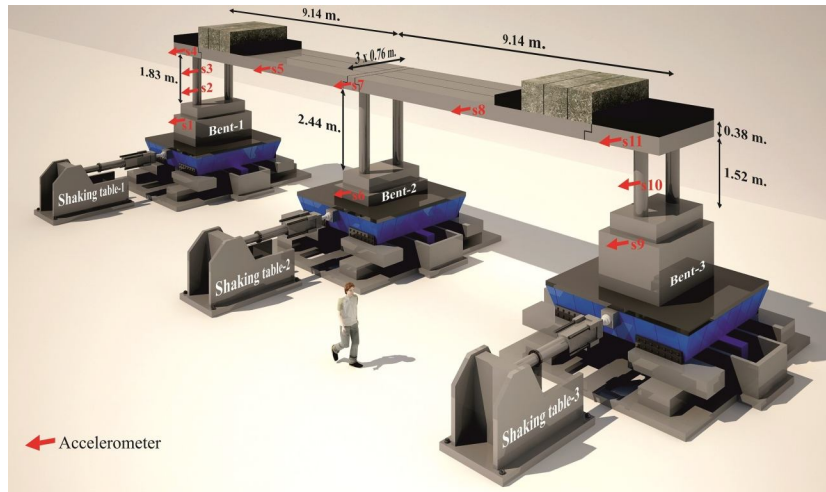
Modal Frequency Information



Modal Identification is performed by Singular Value Decomposition



Vibration-based Seismic Reliability Estimation of a Bridge

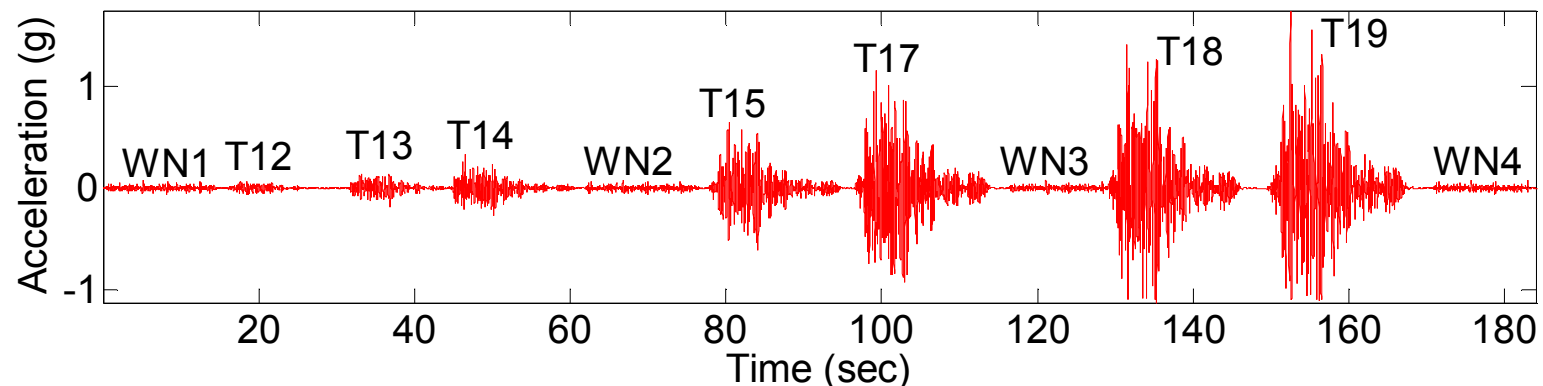


The shaking table test were conducted at University of Nevada, Reno in conjunction with Prof. Saidii's and Prof. Sander's NSF-NEES project.

- Ozer E., Feng M.Q., **Soyoz S.** (2015) "SHM-Integrated Bridge Reliability Estimation using Multivariate Stochastic Processes" *Earthquake Engineering Structural Dynamics*, 44, 601-618.
- Ozer E., **Soyoz S.** (2015) "Vibration-based Damage Detection and Seismic Performance Assessment of Bridges", *Earthquake Spectra*, 31(1), 137-157.
- Soyoz S.**, Feng M.Q., Shinozuka M. (2010) "Remaining Capacity Estimation Based on Structural Identification Results" *Journal of Engineering Mechanics, ASCE*, 136(1), 100-106.
- Soyoz S.**, Feng M.Q. (2008) "Instantaneous Damage Detection of Bridge Structures and Experimental Verification" *Structural Control and Health Monitoring*, 15(7): 958-973.
- Chen Y., Feng M. Q., **Soyoz S.** (2008) "Large-Scale Shake Table Test Verification of Bridge Condition Assessment Methods" *Journal of Structural Engineering, ASCE*, 134(7):1235-1245.

Test Procedure

Test	Ground Motion Description	PGA (g)	Damage Description
WN-1	White Noise in Transverse		
T-13	Low Earthquake in Transverse	0.17	Bent-1 yields
T-14	Moderate Earthquake in Transverse	0.32	Bent-3 yields
WN-2	White Noise in Transverse		
T-15	High Earthquake in Transverse	0.63	Bent-2 yields
WN-3	White Noise in Transverse		
T-19	Extreme Earthquake in Transverse	1.70	Bent-3 steel buckles
WN-4	White Noise in Transverse		



Observed Damage on bent-1

T-13



T-14



T-15



T-19

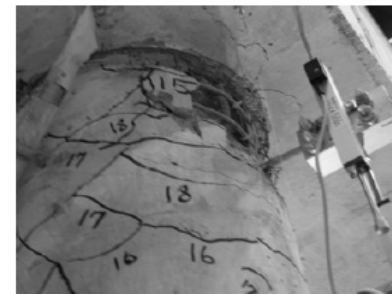


bent-3, T-19

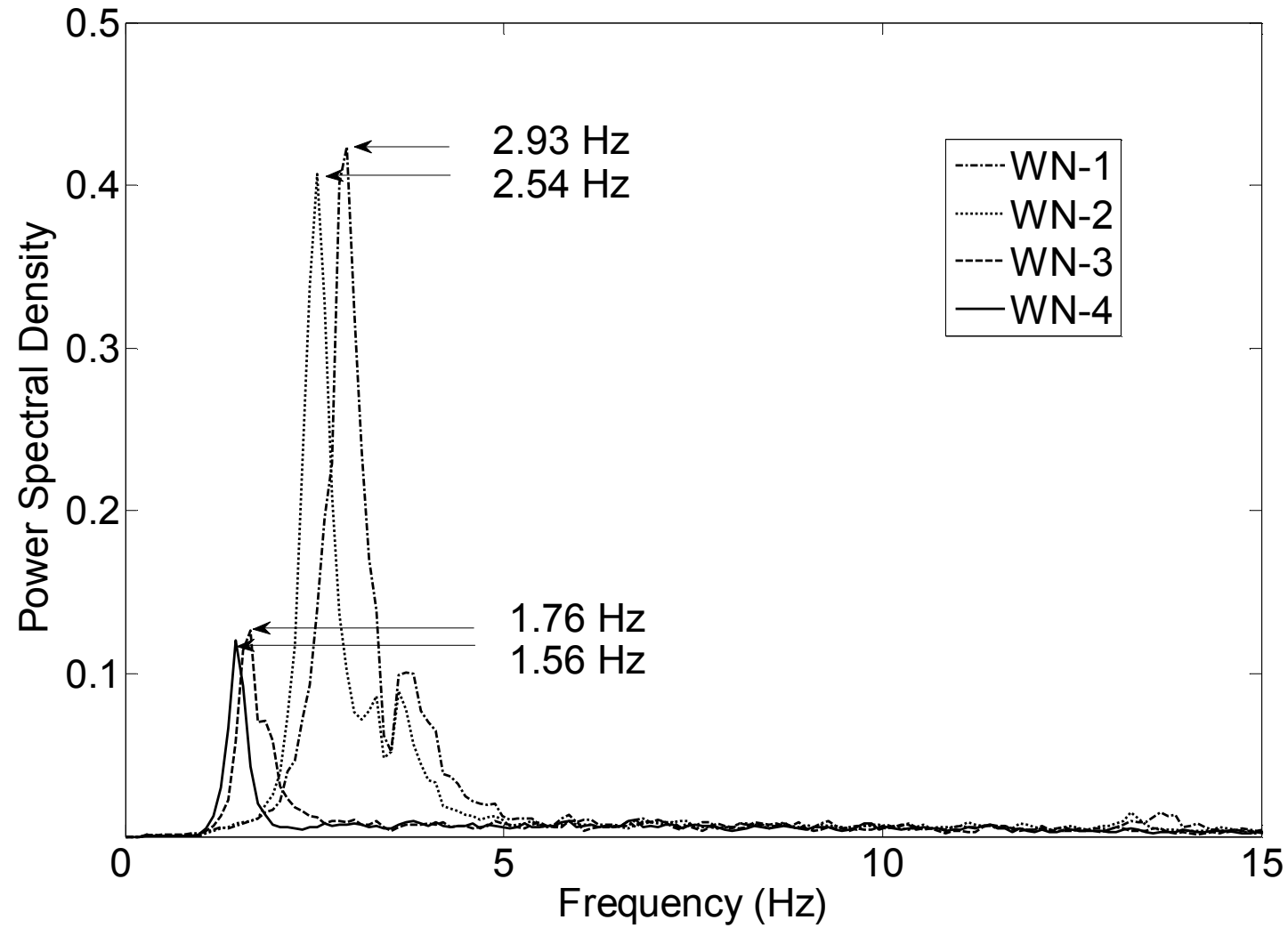
lower (left)



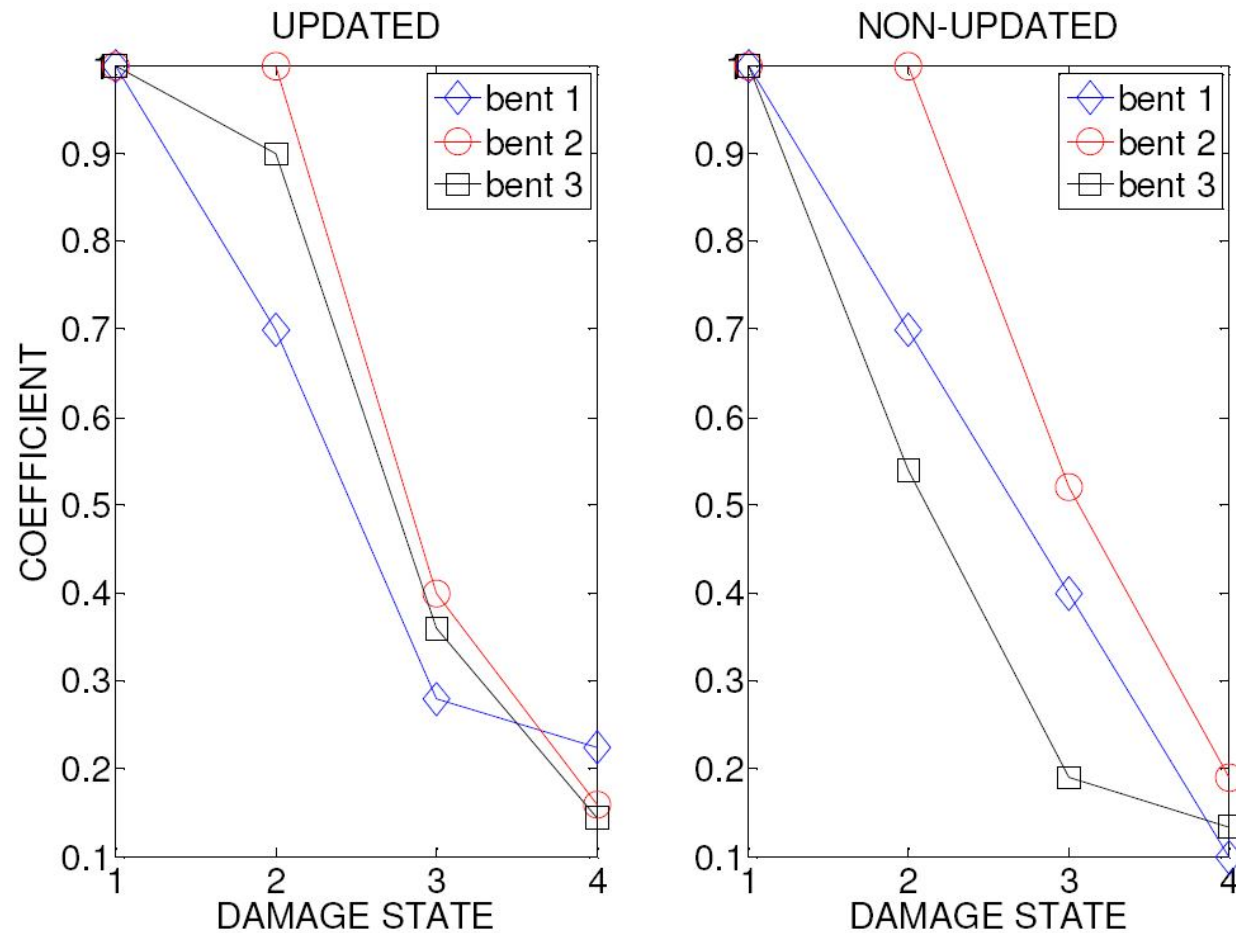
upper (right)



Modal Identification

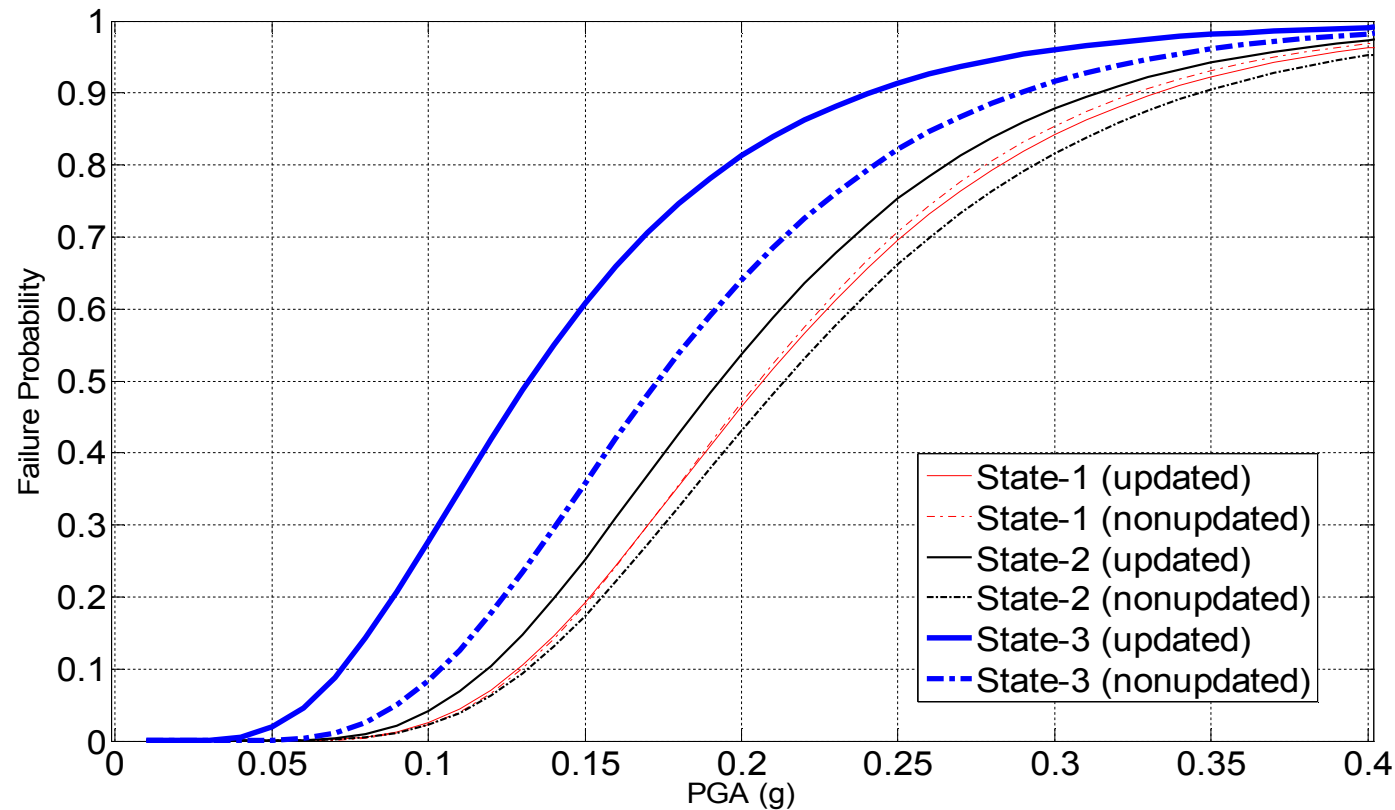


Damage Progress

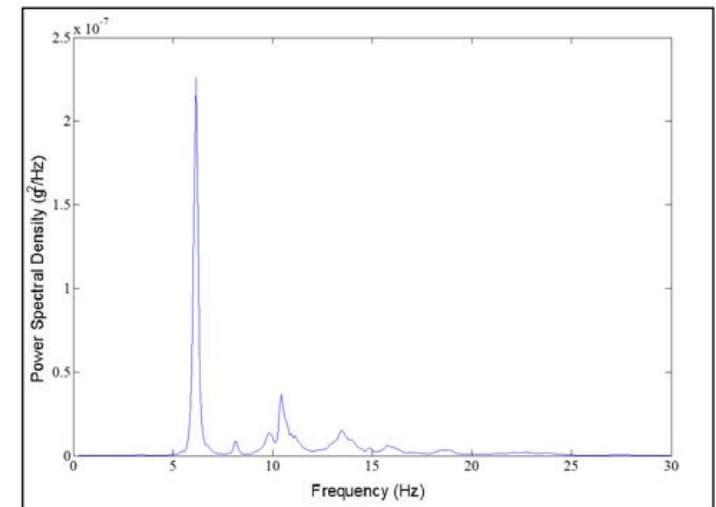
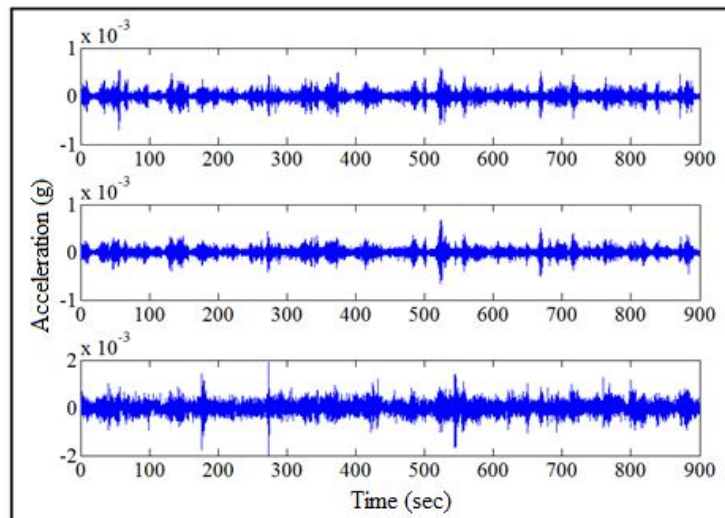
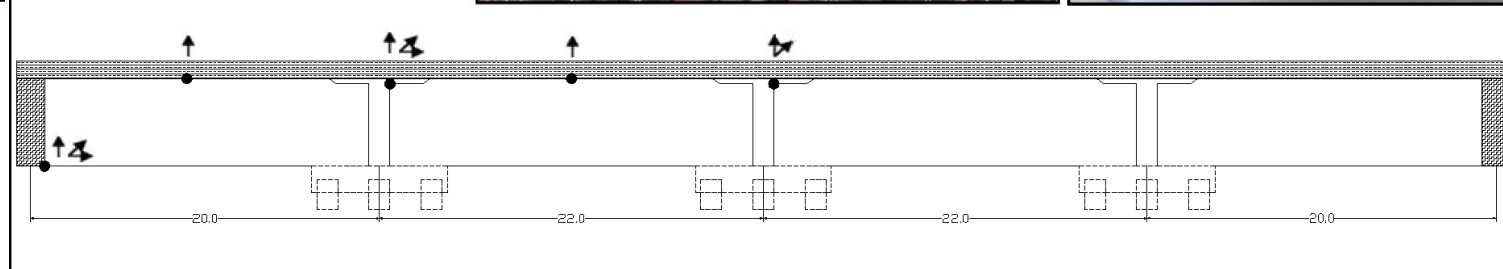
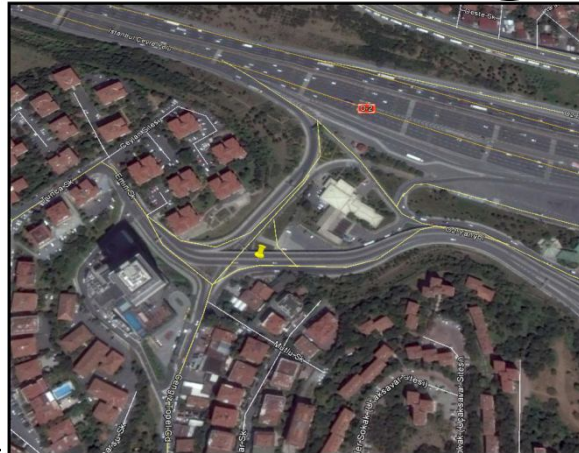


Stiffness values according to different damage states

Effect of System Identification on Reliability Estimation



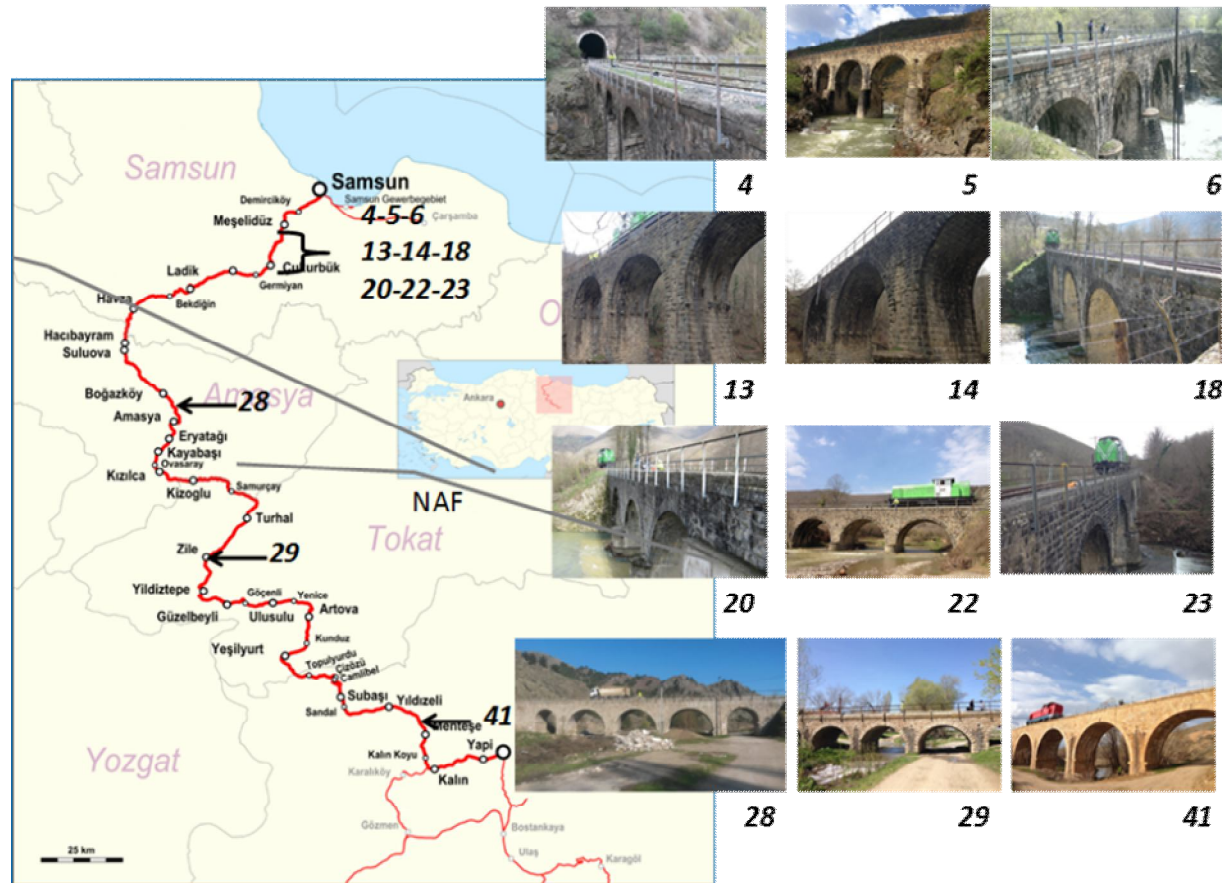
Etiler Bridge



Outline

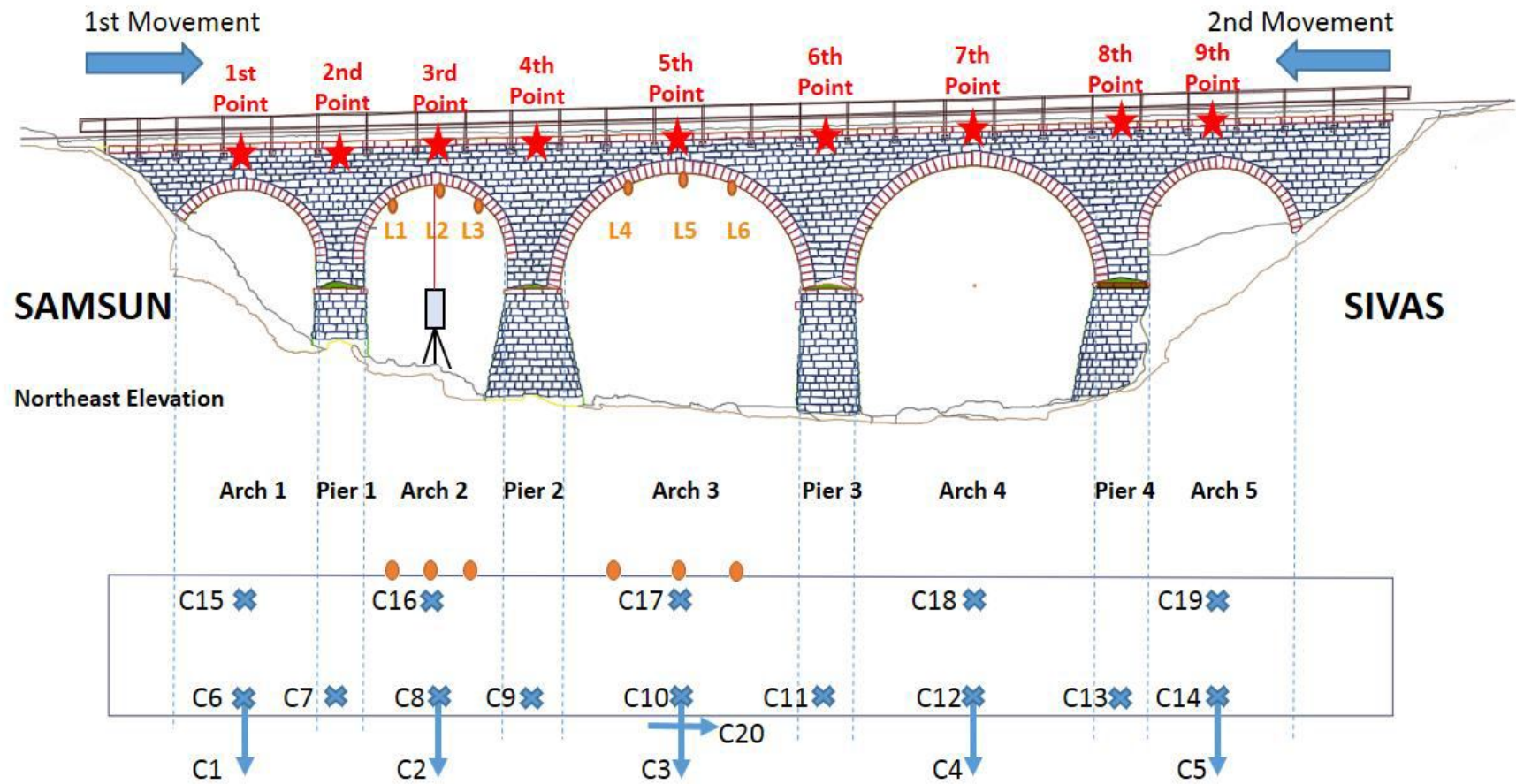
- Structural Health Monitoring
- Some Recents Projects
- Bridge Health Monitoring
 - Highway Bridges
 - Historical Stone Arch Bridges
 - Suspension Bridges

Stone Arch Bridges



Soyoz S. et al (2017) “Dynamic identification-model updating-seismic performance assessment of stone arch bridges” *4th Conf on Smart Monitoring Assessment and Rehabilitation of Civil Structures*, Zurich, Switzerland.

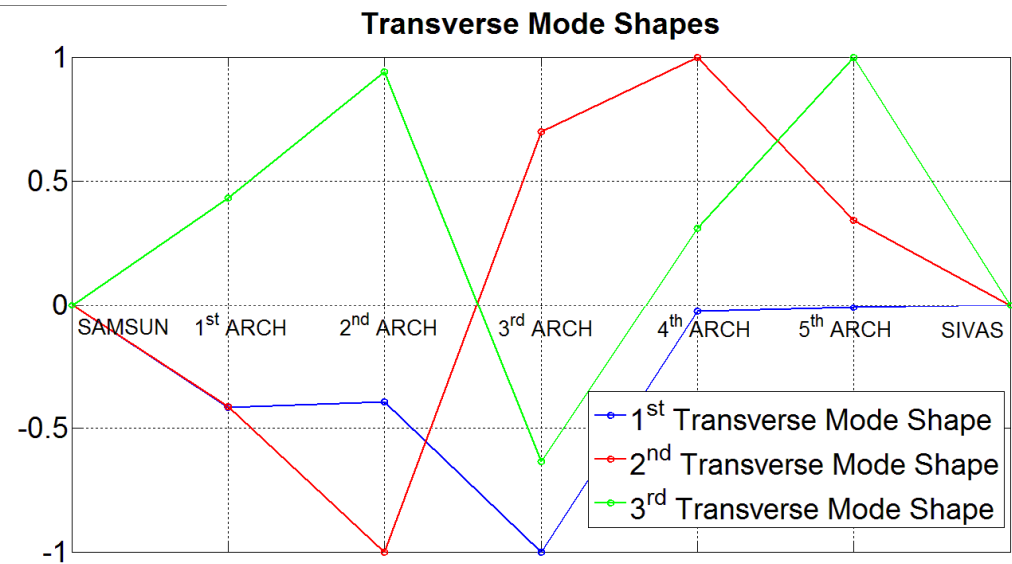
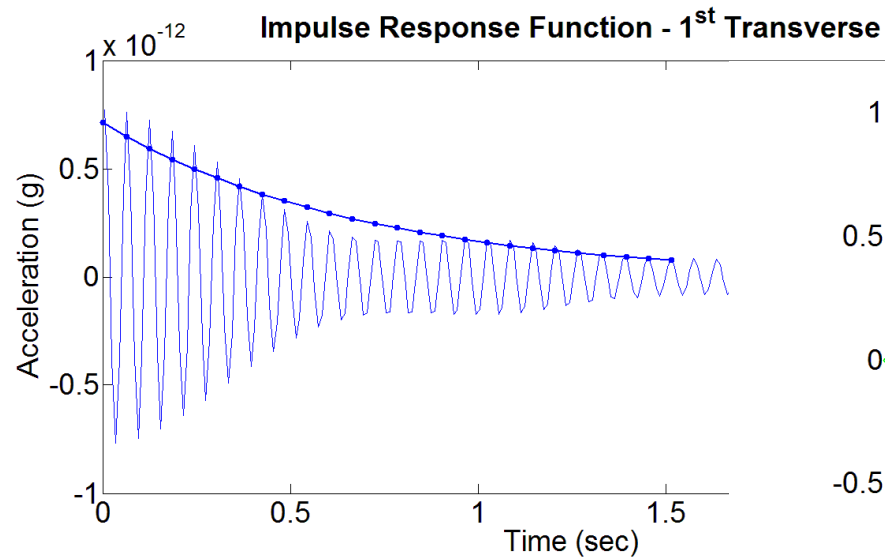
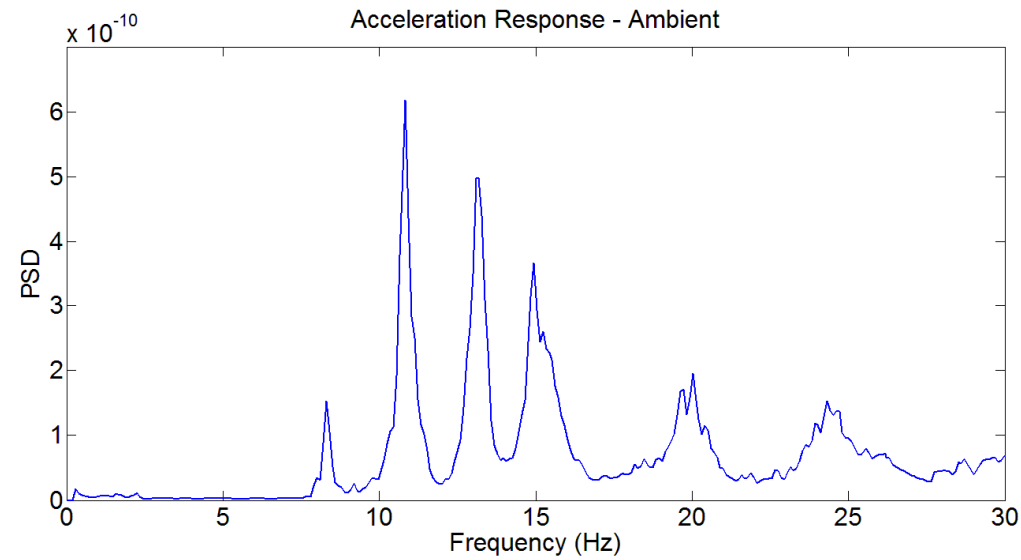
Bridge 6



Ambient Vibration Test



Dynamic Properties



FEM Updating

Modal assurance criteria

Error function

$$MAC = \frac{|\psi_*^T \cdot \psi|^2}{(\psi_*^T \cdot \psi_*) \cdot (\psi^T \cdot \psi)} \quad E = \sum_{i=1}^4 \left(k_i \cdot \left[(f_i^* - f_i) / f_i^* \right]^2 + h_i \cdot [1 - MAC_i]^2 \right)$$

Parameters to be identified

- Young's modulus of stone + mortar
- Soil Springs

FEM Updating

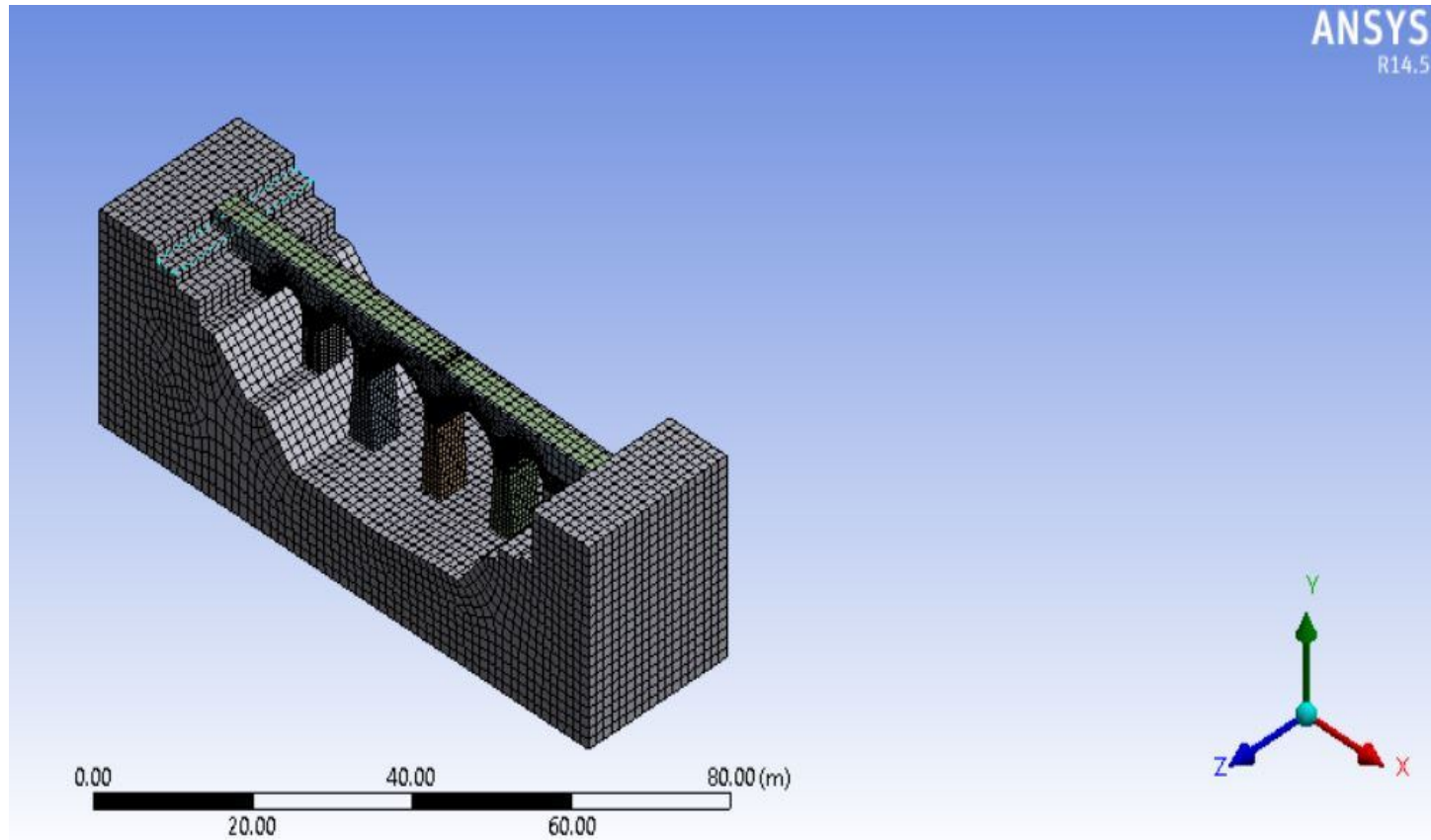
Modal Frequencies

Mode	Non-updated Frequency (Hz)	Updated Frequency (Hz)	Identified Frequency (Hz)
Trans-1	3.28	7.33	8.31
Trans-2	5.79	10.8	10.9
Trans-3	9.29	15.3	13.2
Vert-1	13.0	23.6	20.0
Vert-2	13.8	25.8	24.3

Parameters

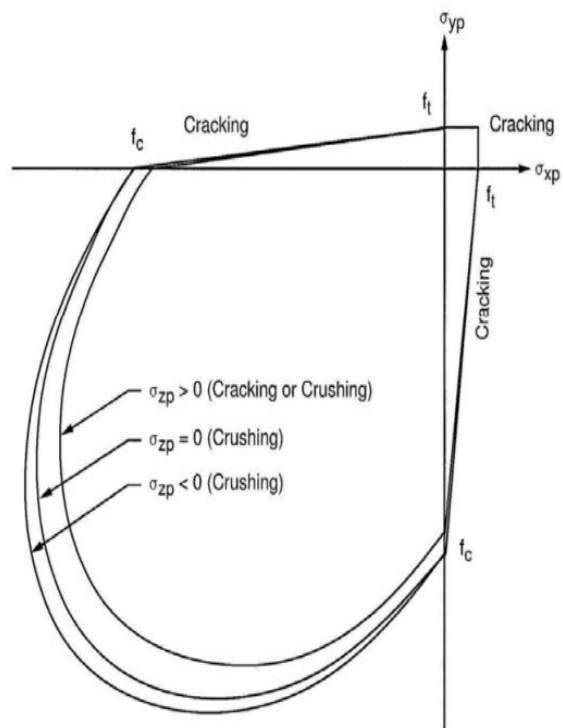
	Non-updated	Updated
E (Gpa)	7.8	12.3
Soil Spring (MN/m)	75	Fixed

ANSYS Model



Nonlinear Model Definition

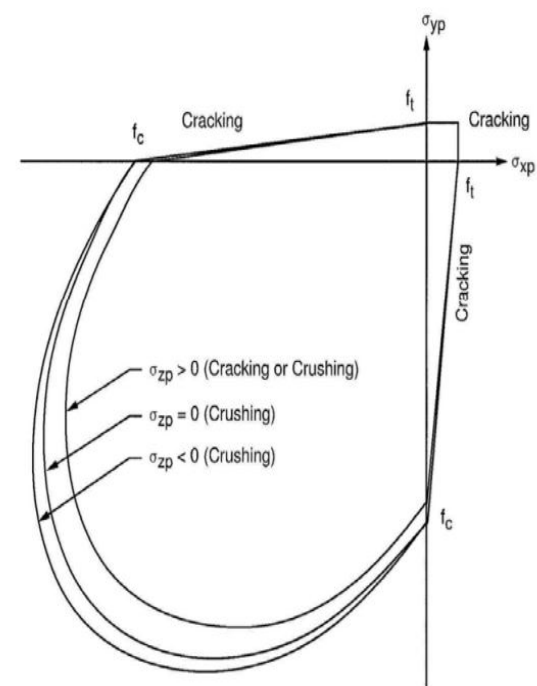
Structure



$f_t = 0.8 \text{ MPa}$

$f_c = 56.5 \text{ MPa}$

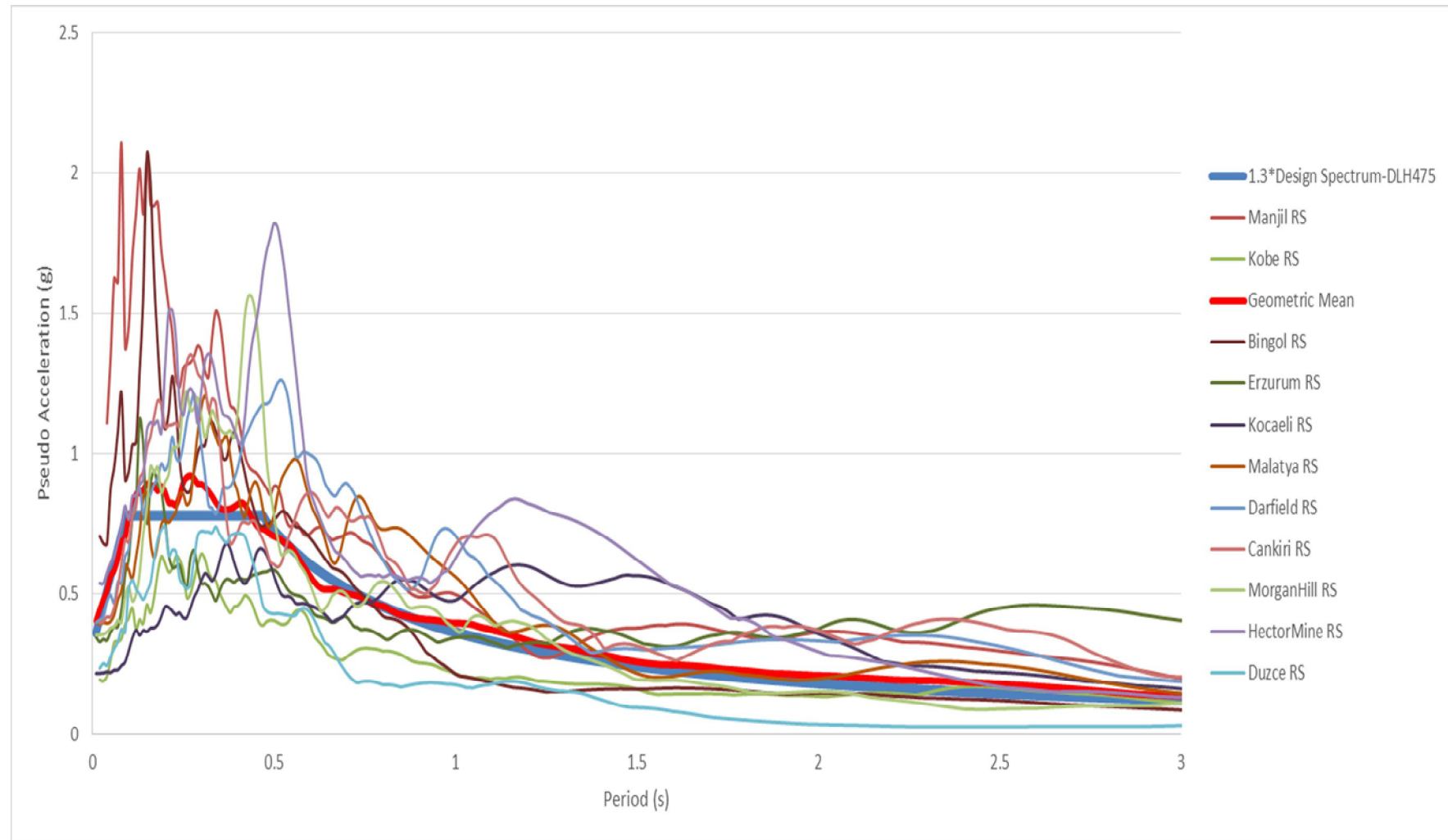
Soil



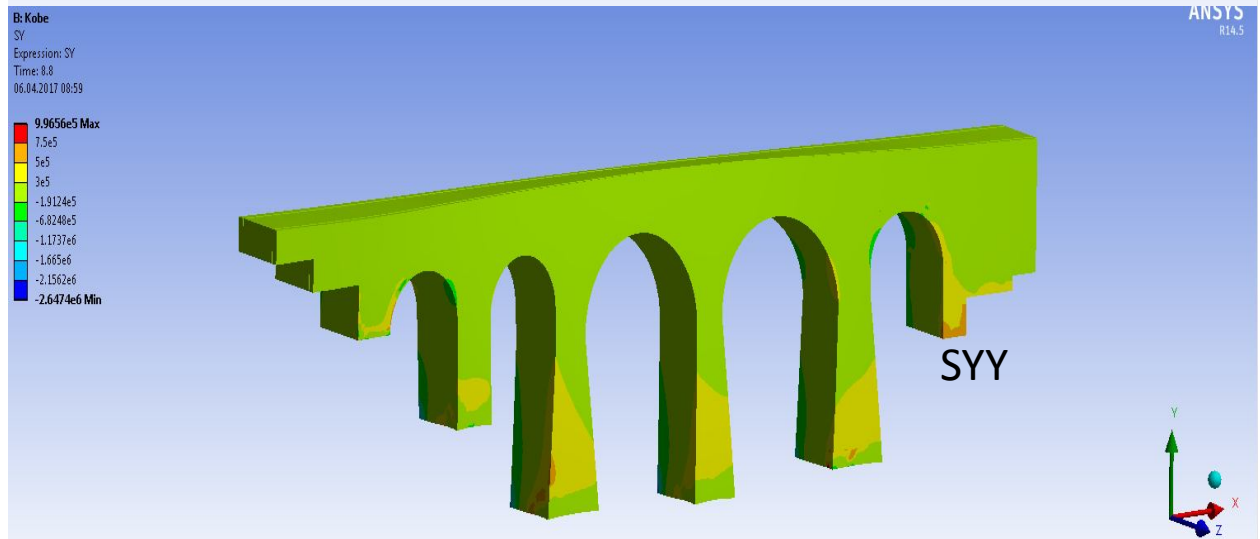
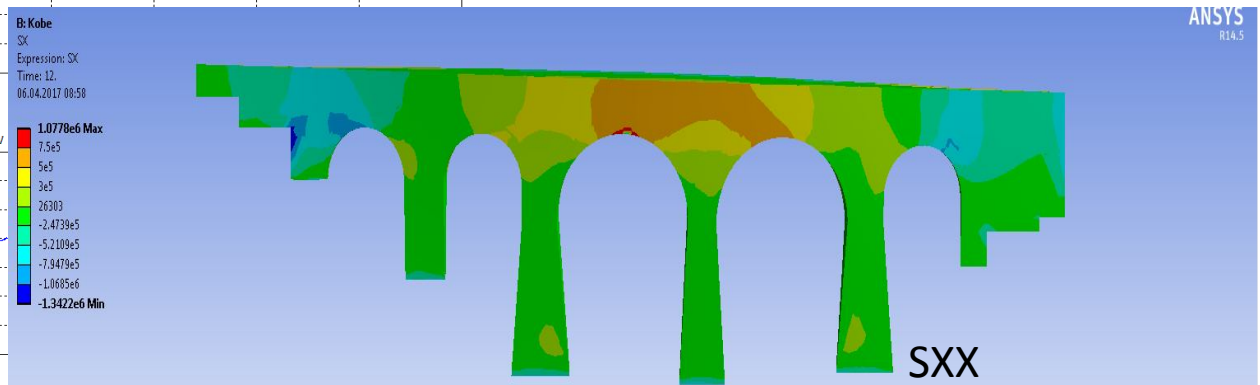
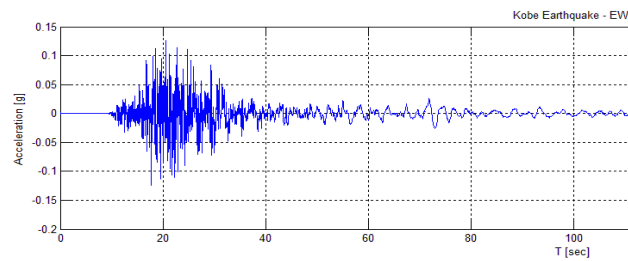
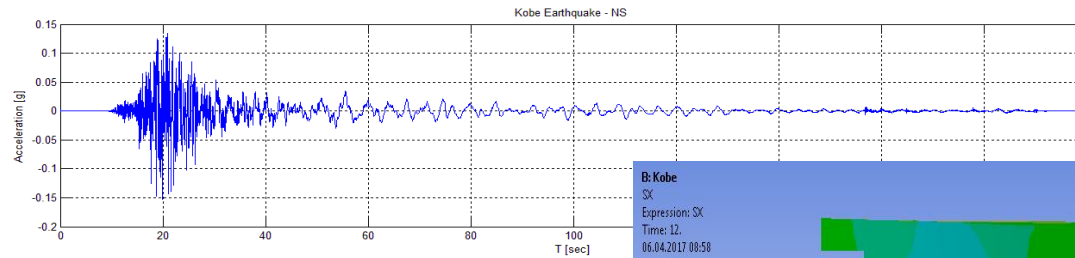
$f_t = 0.1 \text{ MPa}$

$f_c = 10 \text{ MPa}$

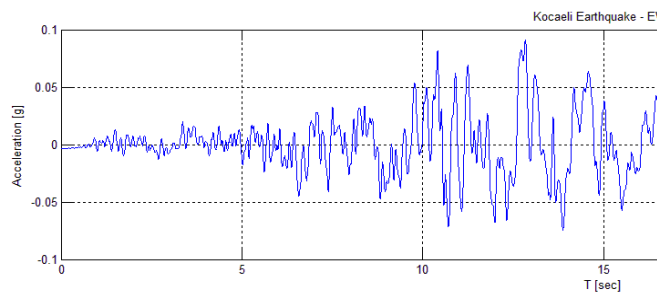
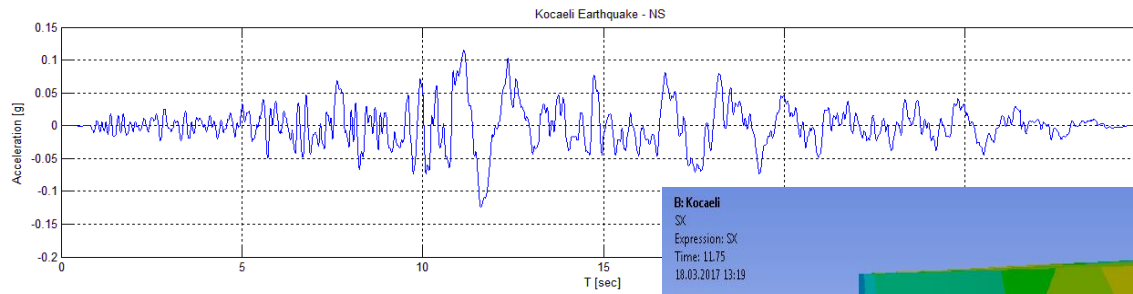
Seismic Input



Kobe Earthquake

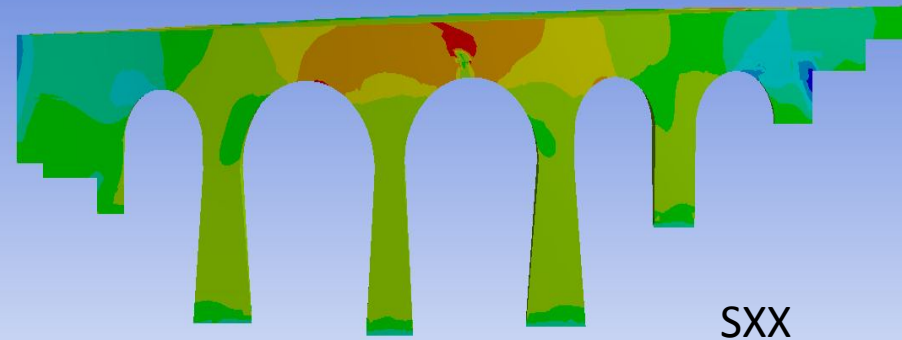


Kocaeli Earthquake



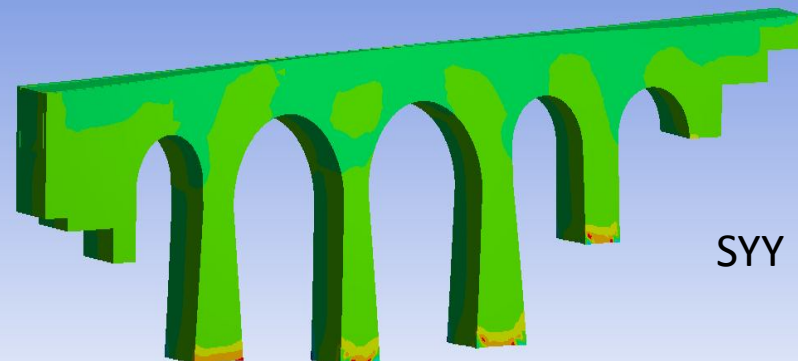
B: Kocaeli
SX
Expression: SX
Time: 11.75
18.03.2017 13:19

1.0977e6 Max
7.5e5
5e5
3e5
-28693
-3.5739e5
-6.8608e5
-1.0140e6
-1.3435e6
-1.6722e6 Min



B: Kocaeli
SY
Expression: SY
Time: 7.68
18.03.2017 13:54

1.0673e6 Max
7.5e5
5e5
3e5
-1
-2.3159e5
-4.6311e5
-6.9476e5
-9.2635e5 Min



Conclusion

- System identification for “global” structural condition assessment
- Vibration-based FEM updating of structures
- Seismic Reliability Analysis with updated FEM

Outline

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 - Historical Stone Arch Bridges
 - Suspension Bridges

Suspension Bridges-California



81 sensors



53 sensors



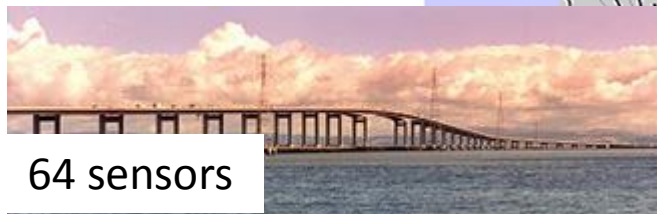
11 sensors



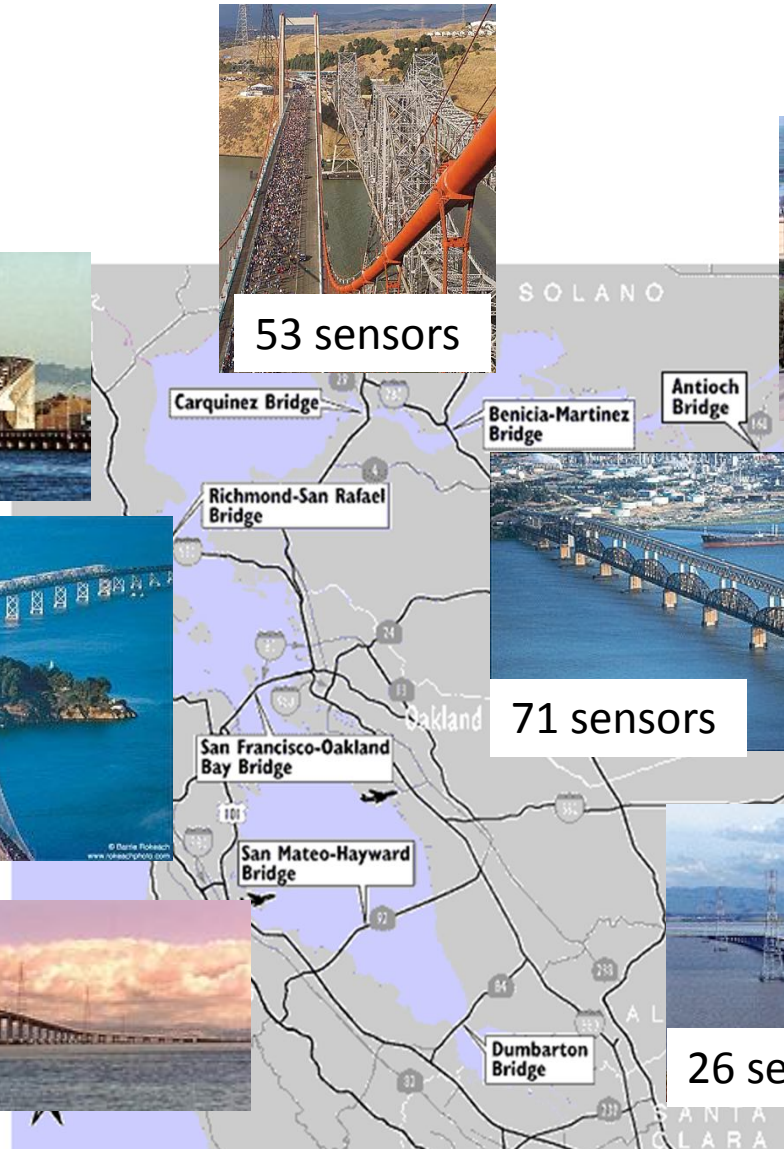
64 sensors



71 sensors



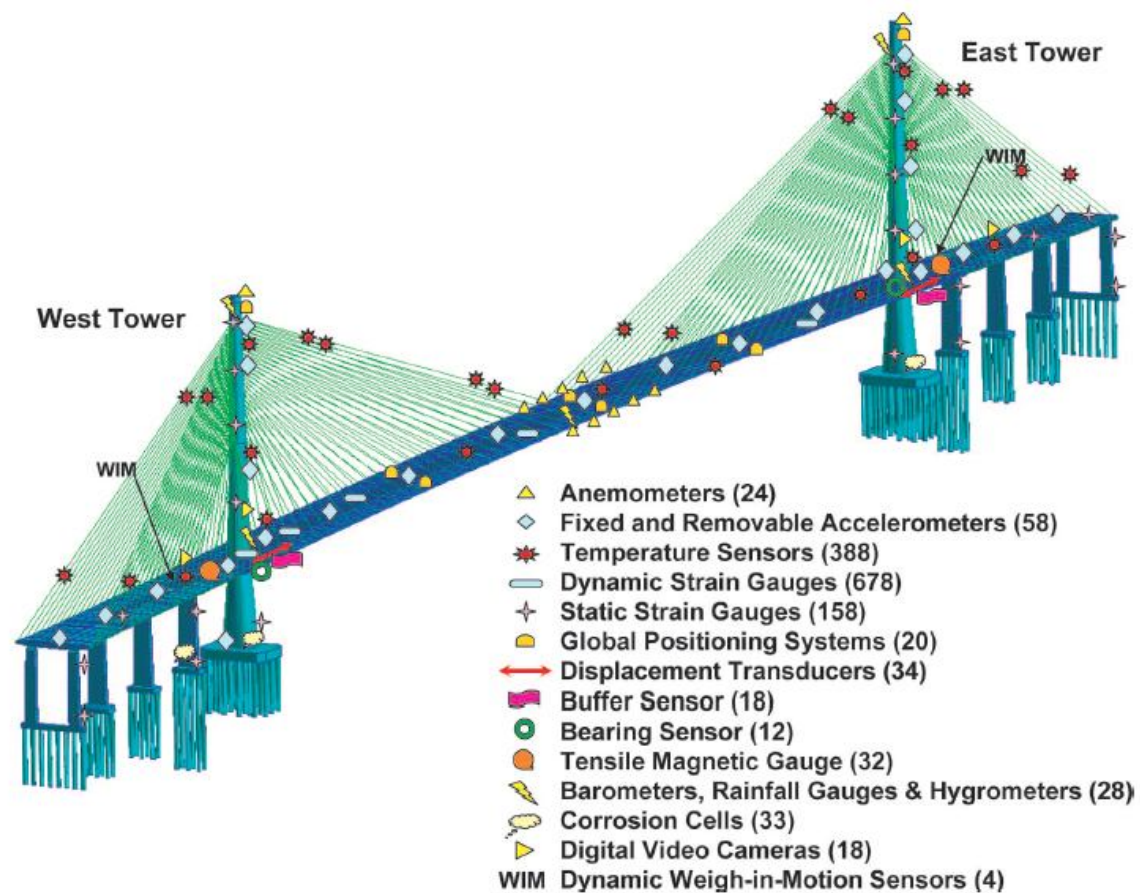
26 sensors



Design of SHM systems for long-span bridges

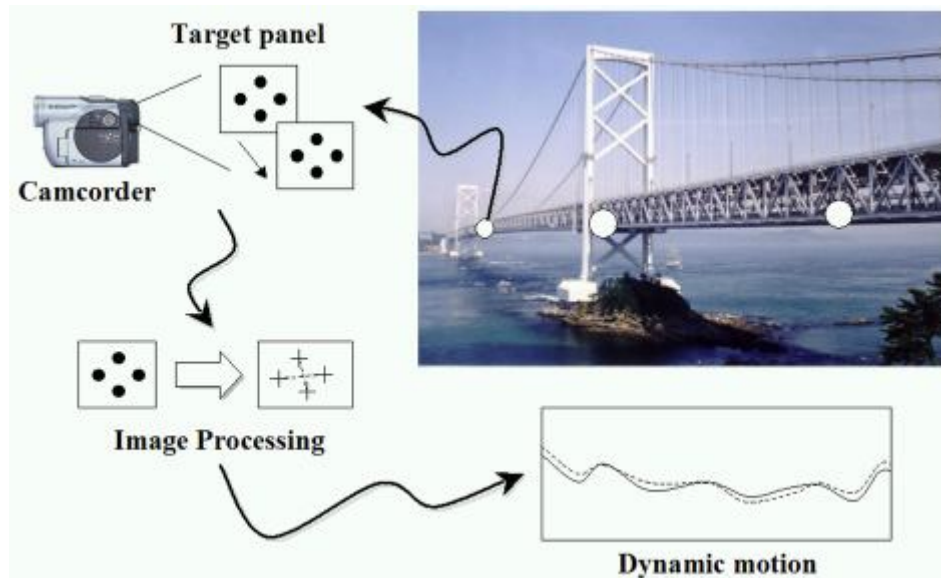
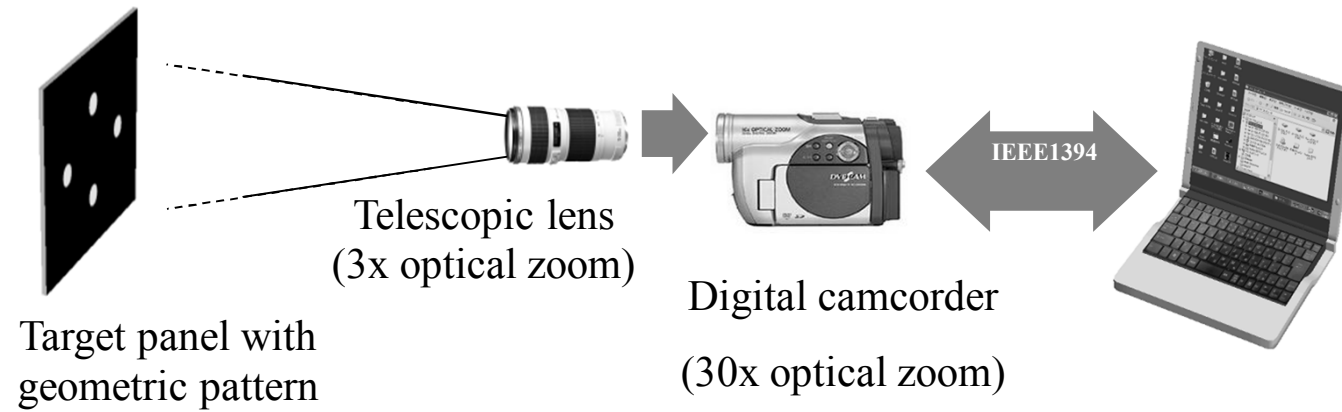
Wong K-Y

Structure and Infrastructure Engineering, 2007



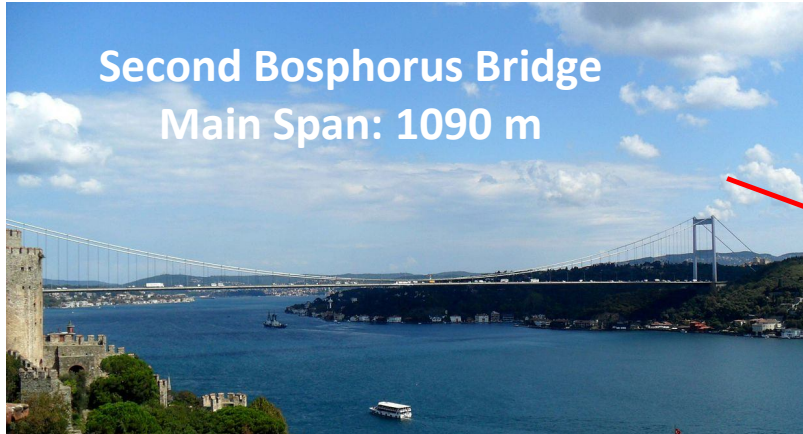
Stonecutters bridge

Optical Sensors



Suspension Bridges in Turkey

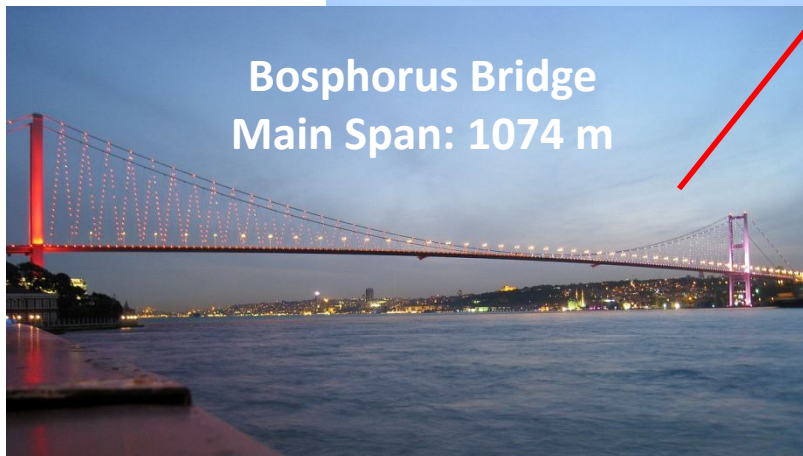
Second Bosphorus Bridge
Main Span: 1090 m



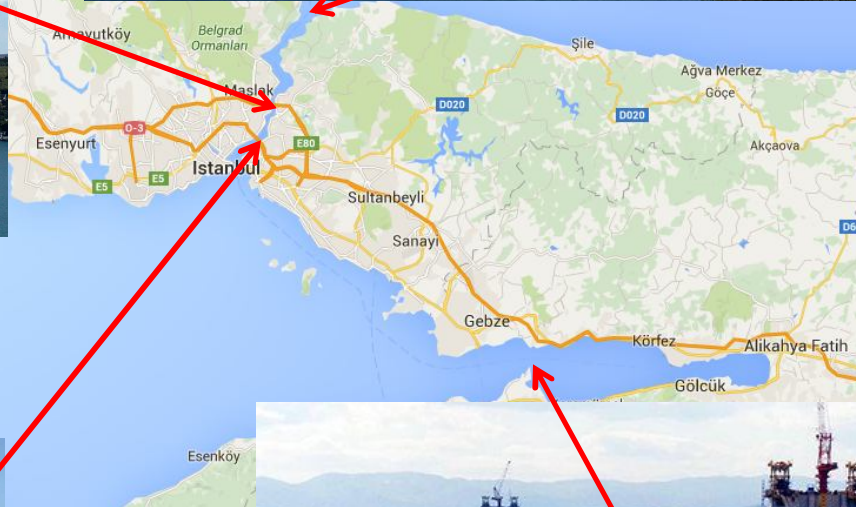
Third Bogazici Bridge
Main Span: 1408 m



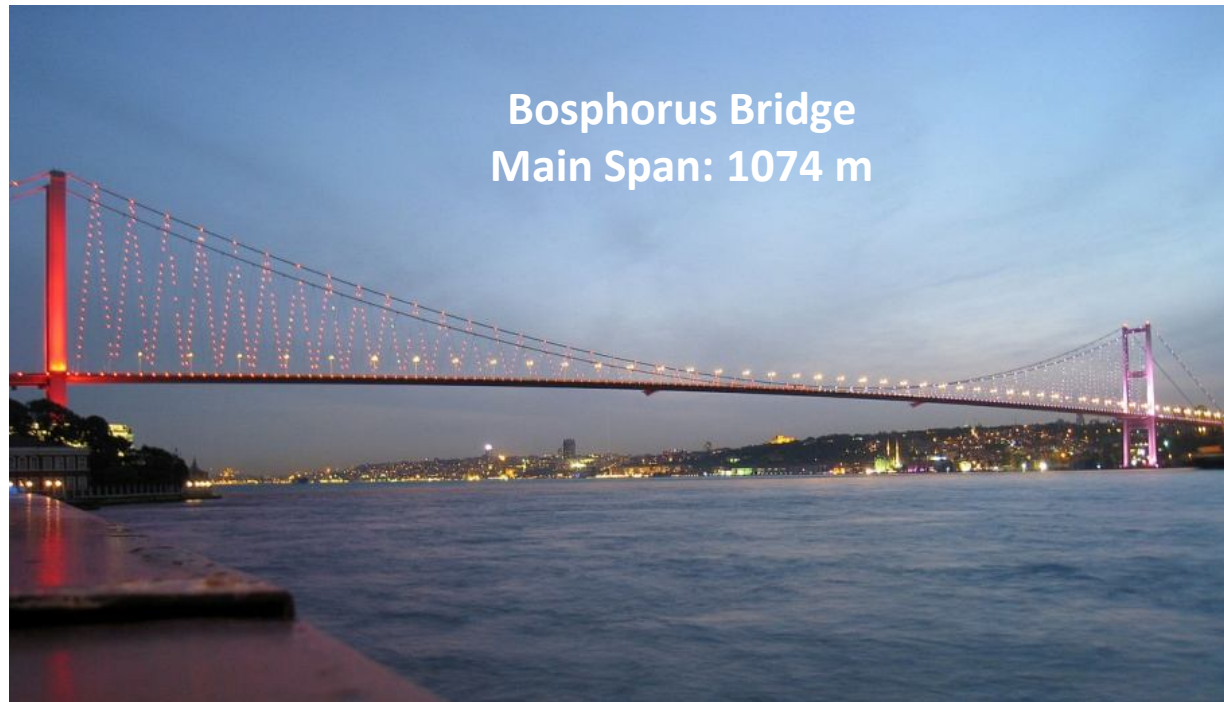
Bosphorus Bridge
Main Span: 1074 m



Izmit Bay Bridge
Main Span: 1550 m

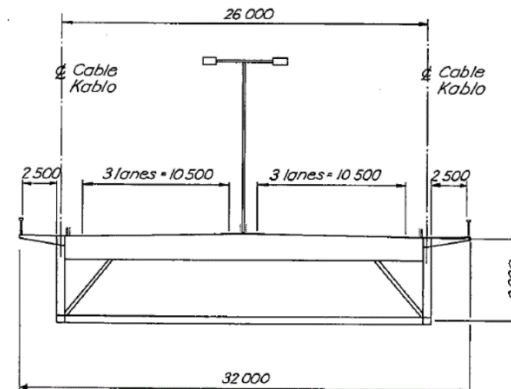
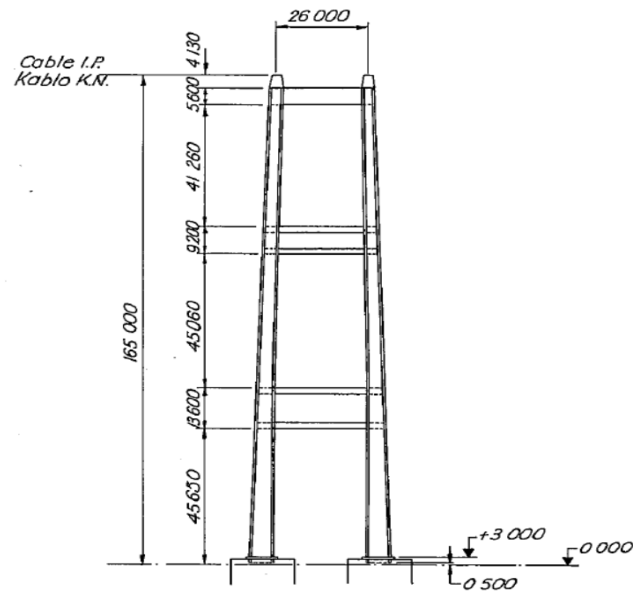


Hanger Replacement of Bogazici Bridge



Soyoz S. et al (2017) "System identification of Bogazici suspension bridge during hanger replacement" *10th Conf on Structural Dynamics*, Rome, Italy.

-Completed in 1974-



Change of Hangers-Inclined to Vertical

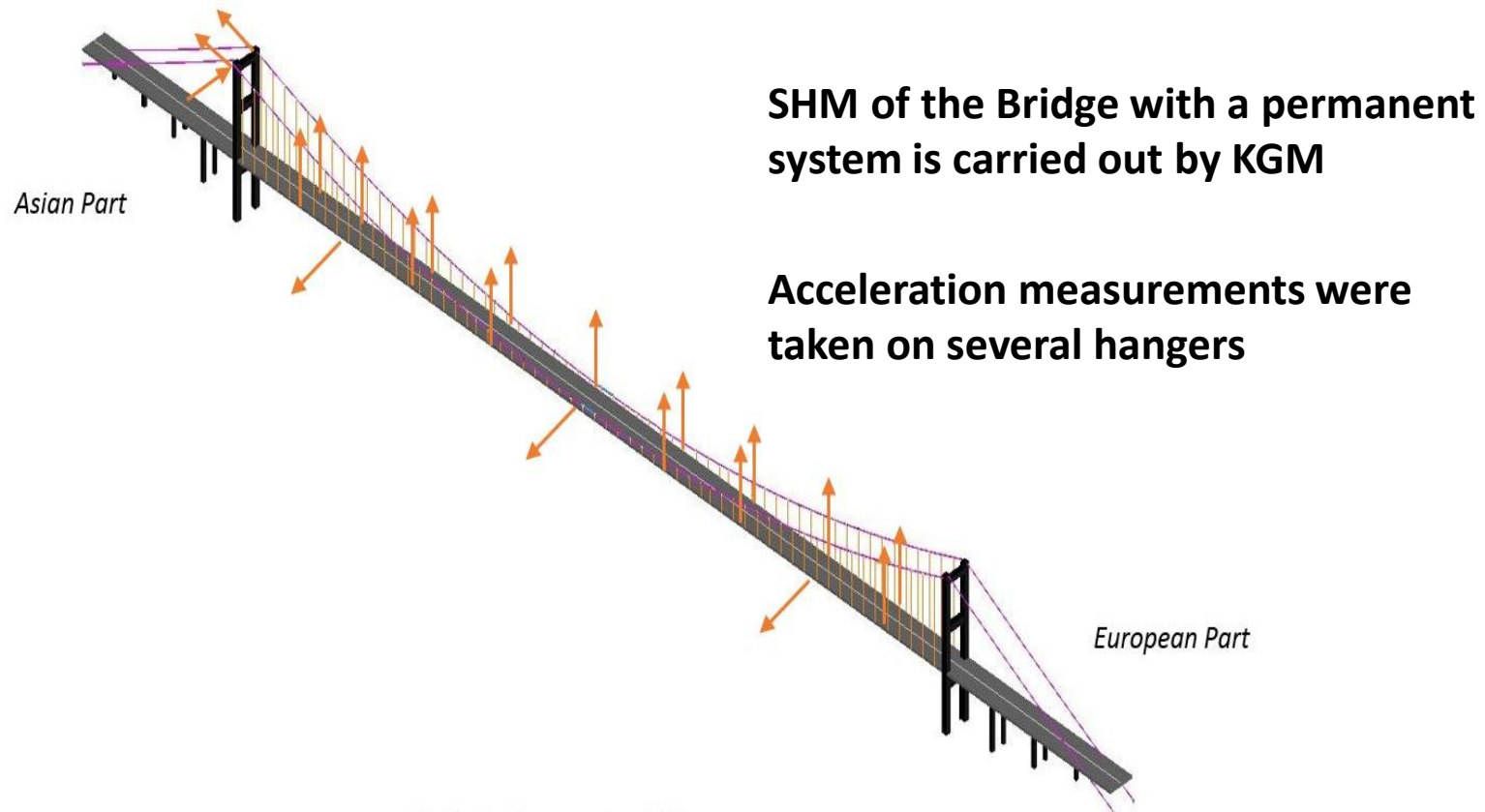


Change of Hangers-Inclined to Vertical



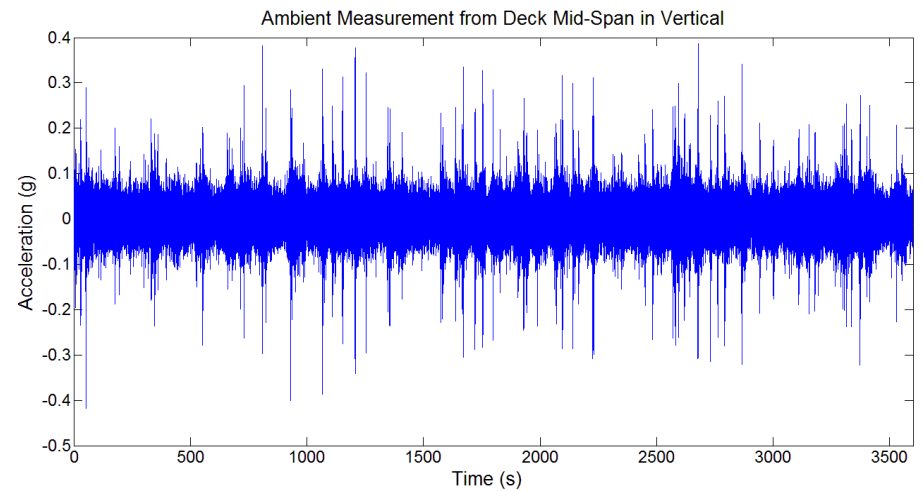
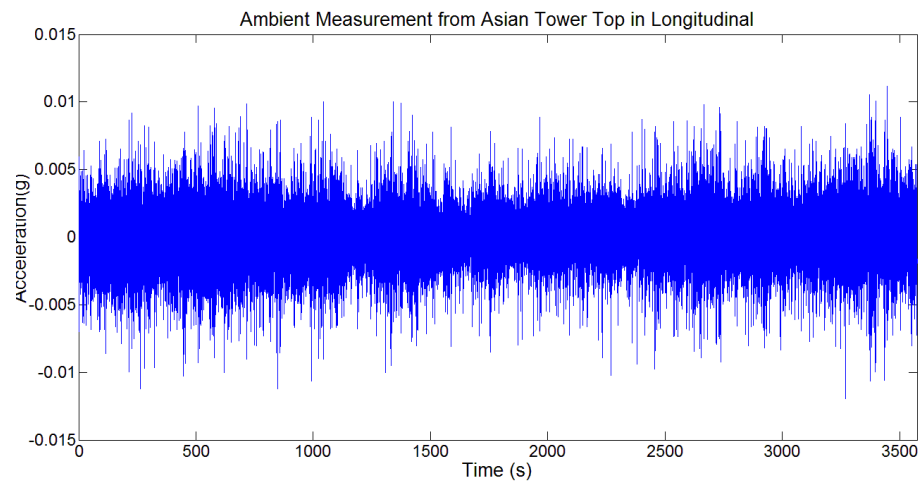
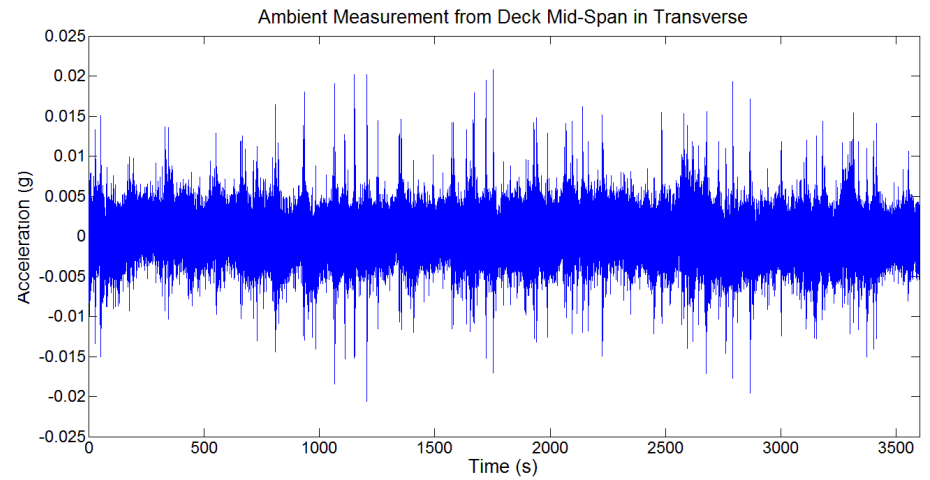
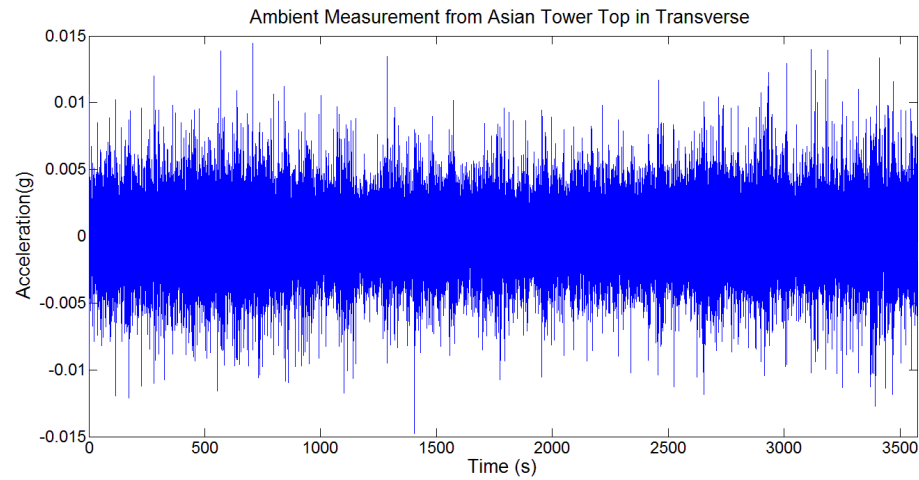
System Identification

Instrumentation



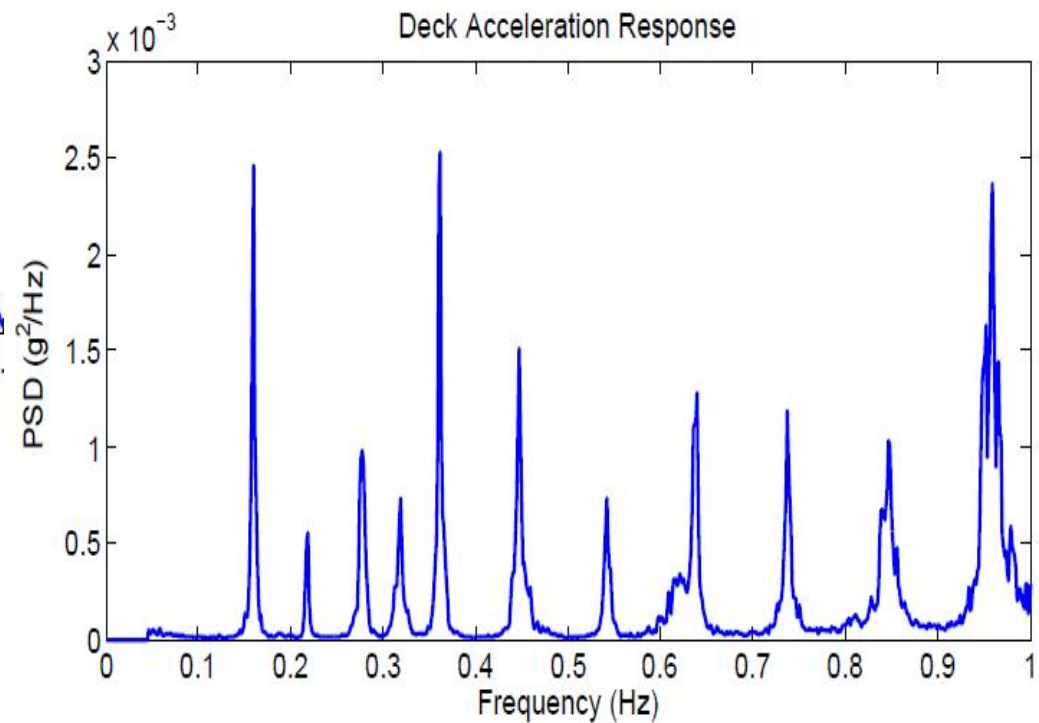
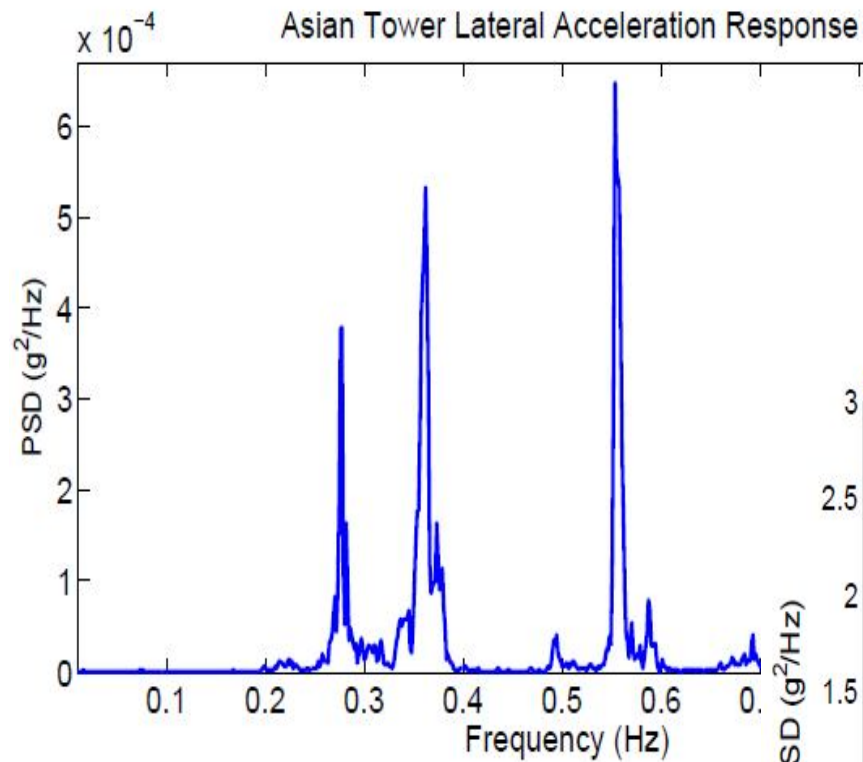
System Identification

Measurement



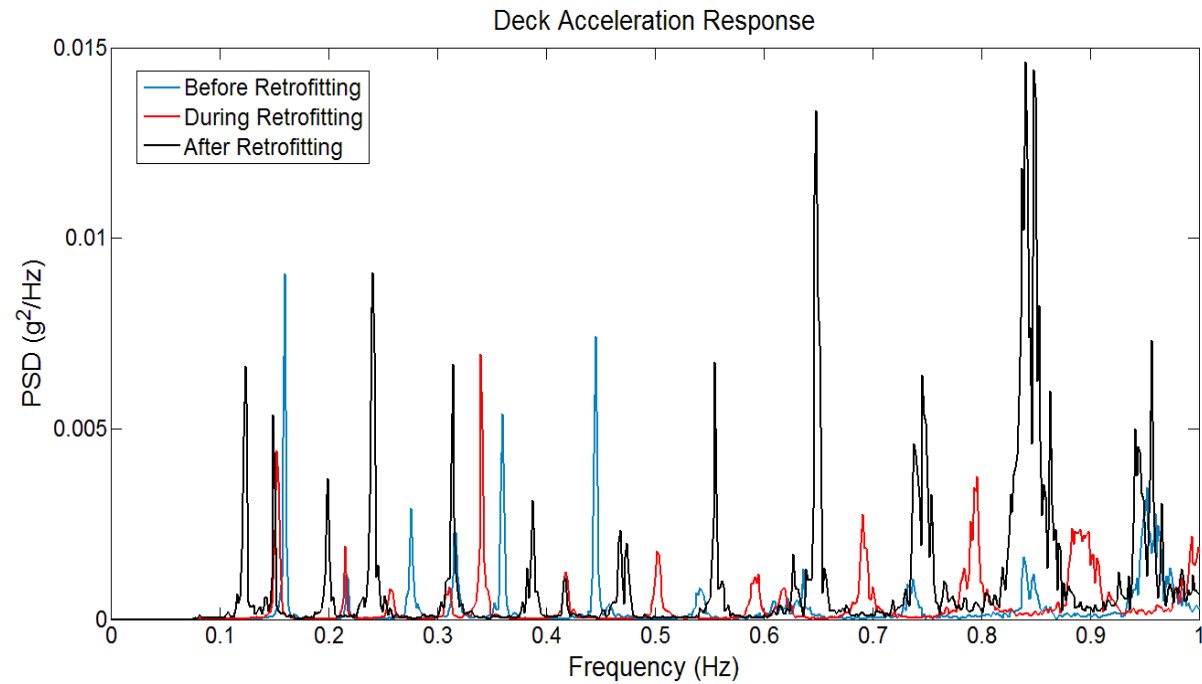
System Identification

Frequency Response



System Identification

Effect of Retrofitting

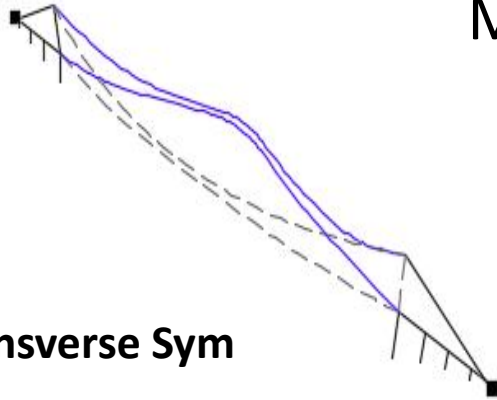


Mod Number	Before Retrofitting	During Retrofitting	After Retrofitting	Difference (%)
1 (1st Trans)	0.074 Hz	0.076 Hz	0.081 Hz	9.5
2 (1st Vasy)	0.149 Hz	0.137 Hz	0.125 Hz	16.1
3 (1st Vsym)	0.159 Hz	0.154 Hz	0.149 Hz	6.3
4 (2nd Vsym)	0.217 Hz	0.215 Hz	0.201 Hz	7.4
5 (3rd Vasy)	0.276 Hz	0.262 Hz	0.243 Hz	12.0

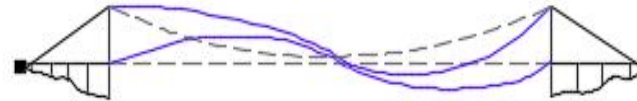
System Identification

Mode Shapes

1st Transverse Sym



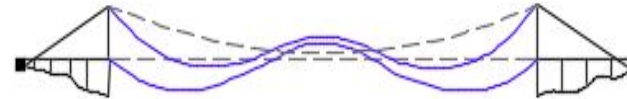
1st Vertical Asym



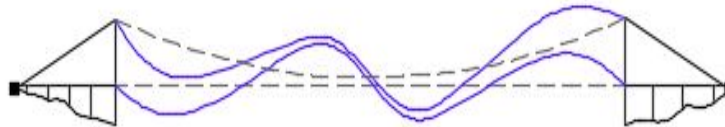
1st Vertical Sym



2nd Vertical Sym

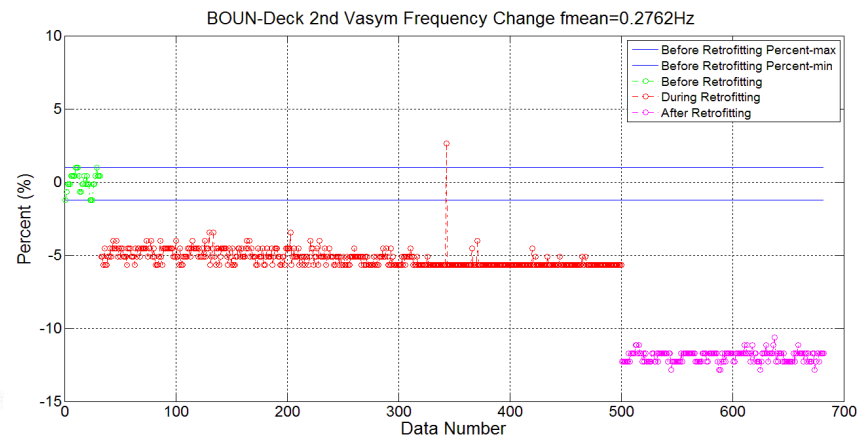
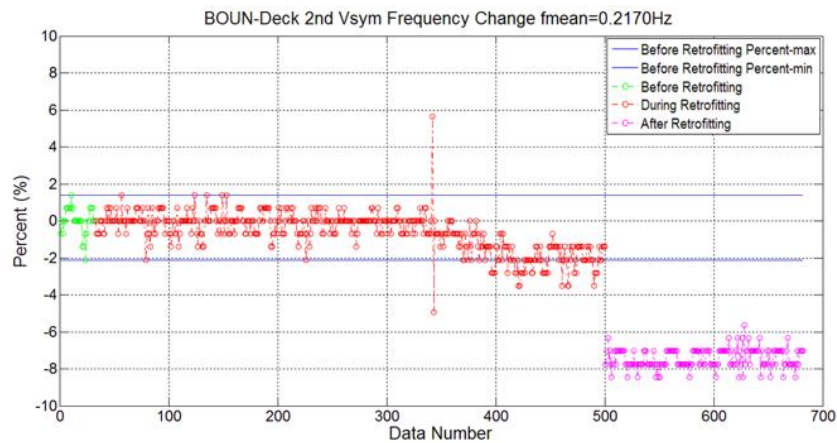
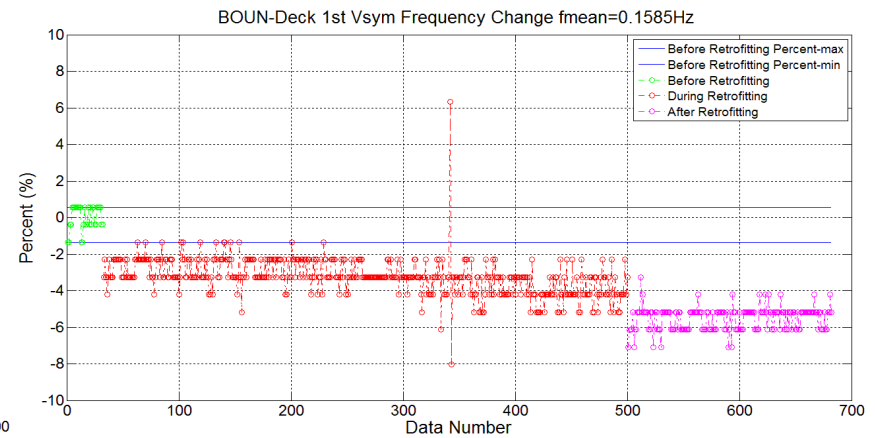
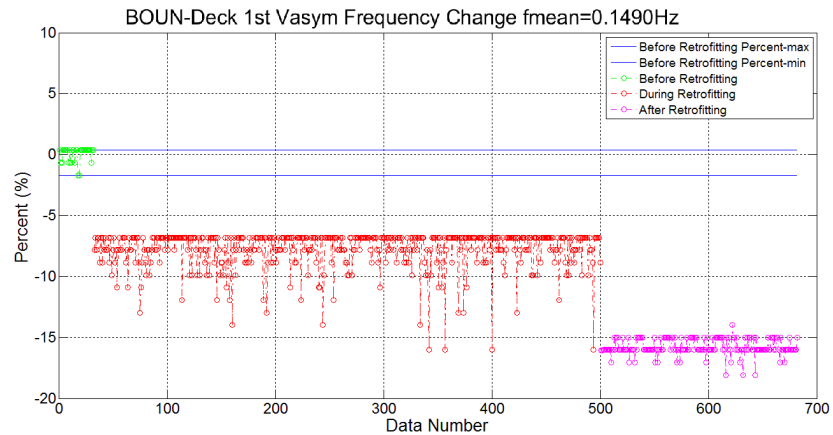


2nd Vertical Asym



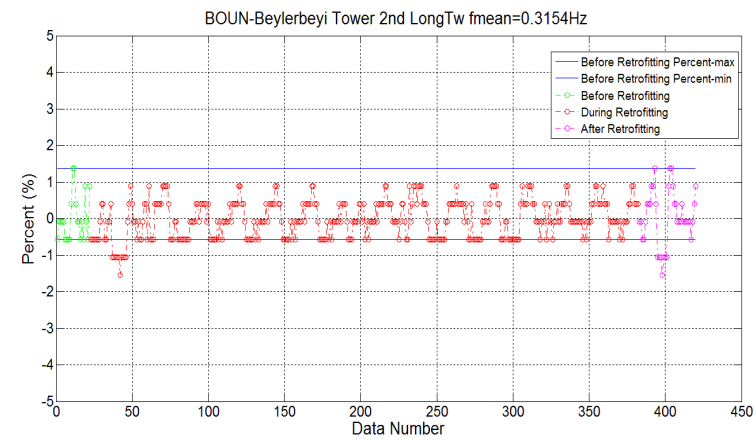
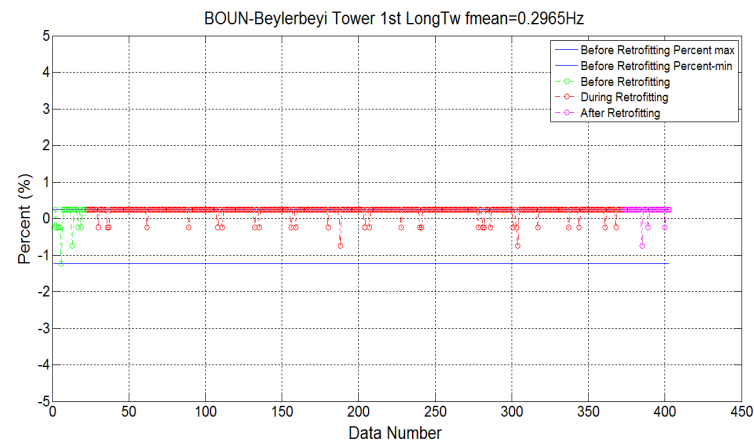
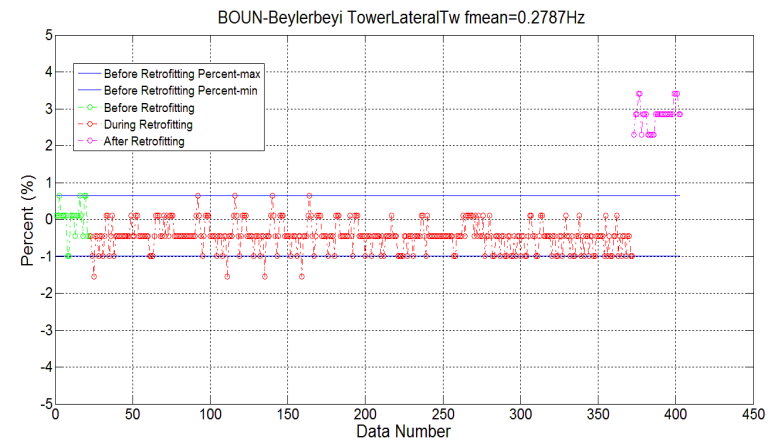
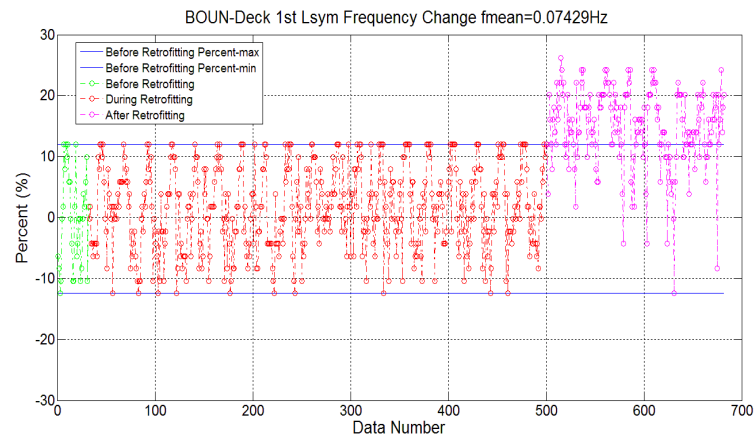
System Identification

Long-Term Monitoring



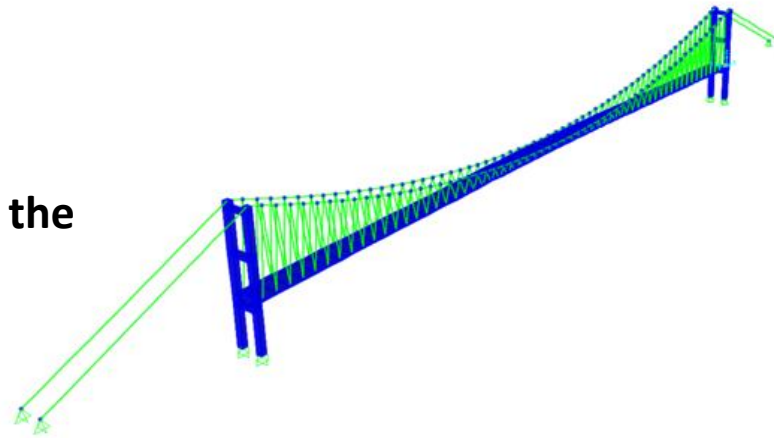
System Identification

Long-Term Monitoring

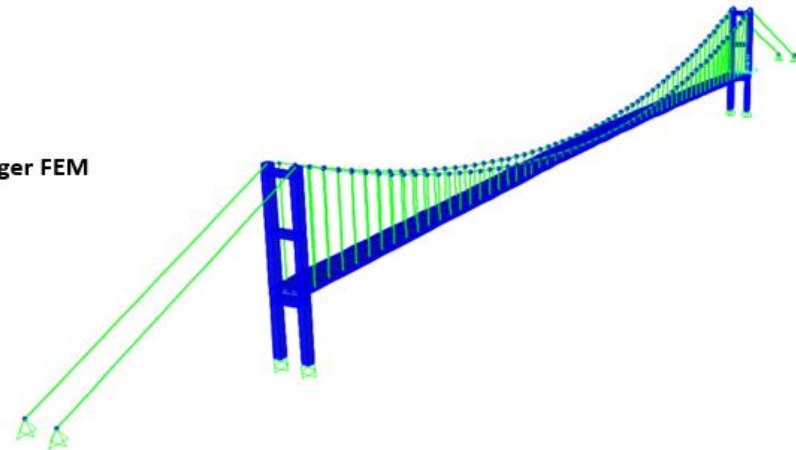


Finite Element Model

Initial strains were introduced to cables and hangers to obtain representative deformed shape of the bridge after dead load analysis



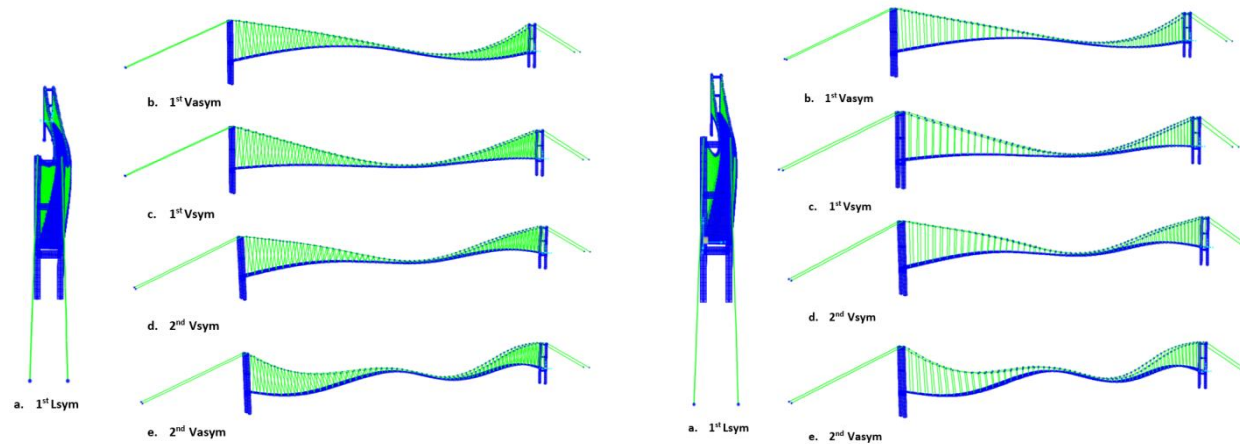
a. Inclined Hanger FEM



b. Vertical Hanger FEM

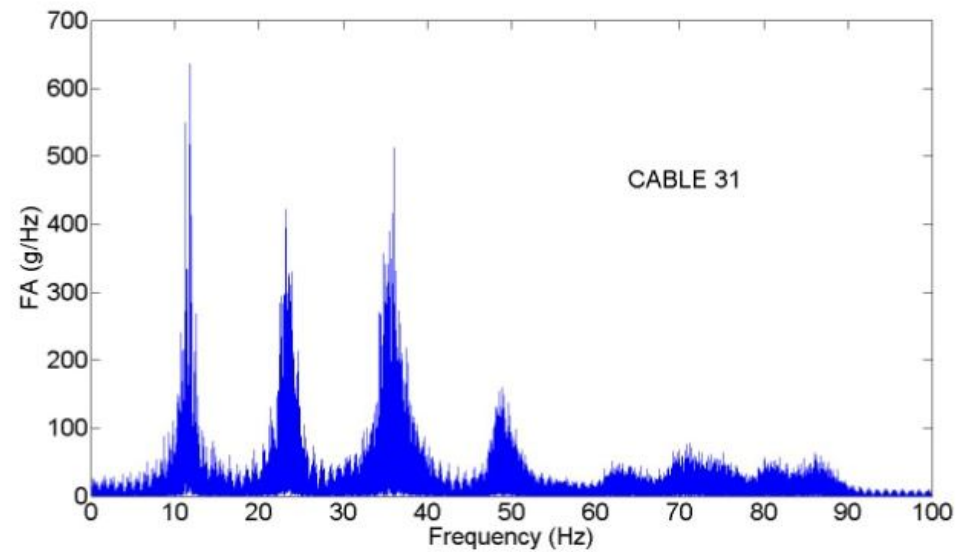
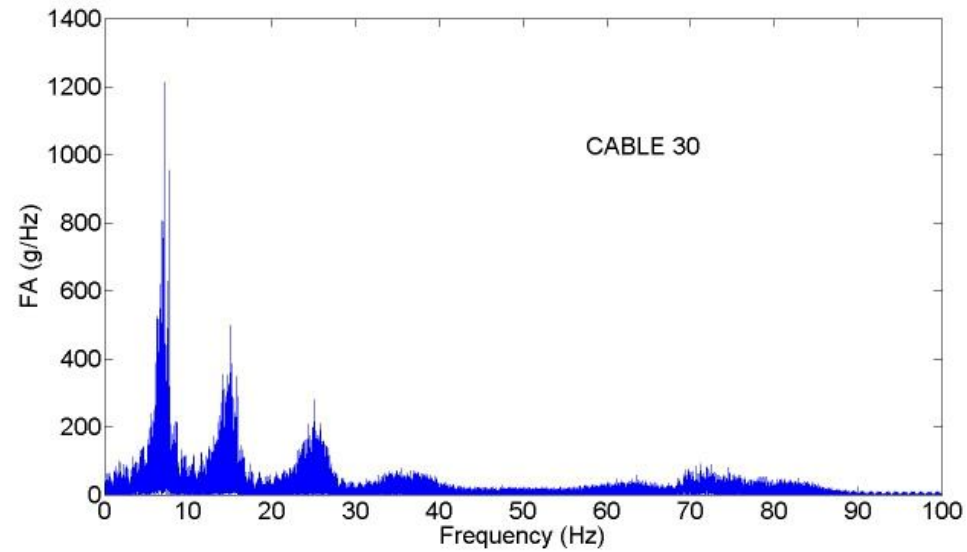
Tension forces of inclined cables at the forth pair are 449.5 kN and 776.8 kN.
And, those of each vertical cable at the same pair are equal and 599.1 kN.

Finite Element Model



Mode Shapes	Natural Modal Frequencies (Hz)		Difference (%)
	Inclined Hanger FEM	Vertical Hanger FEM	
1 (1st Trans)	0.073	0.072	1.4
2 (1st Vasy)	0.138	0.129	6.5
3 (1st Vsym)	0.174	0.165	5.2
4 (2nd Vsym)	0.234	0.219	6.4
5 (2nd Vasy)	0.296	0.269	9.1

Hanger Frequencies



Conclusions

- Vibration based monitoring of Bogazici Bridge during change of hangers from inclined to vertical was carried out almost for one year
- Clear decrease in the vertical modal frequencies of the deck
- Good agreement between FEM and System ID results

Thank you for your attention